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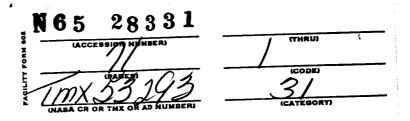
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SA-10 FLIGHT MECHANICAL SUMMARY

by AERO-ASTRODYNAMICS LABORATORY

NASA



George C. Marshall Space Flight Center, Huntsville, Alabama

TECHNICAL MEMORANDUM X-53293

SA-10 FLIGHT MECHANICAL SUMMARY

George C. Marshall Space Flight Center

ABSTRACT

2833/

This report presents the Flight Mechanical Summary for Saturn I vehicle SA-10 to be launched from Pad 37B, Eastern Test Range on a flight azimuth of 95.2 degrees East-of-North. A successful flight will insert the spent S-IV stage and payload consisting of an Apollo boilerplate (BP-9) and a Meteoroid Technology Satellite (Pegasus C) into a 535 km circular orbit. Included is a discussion of the operational predicted trajectory with its orbital mission objectives and constraints, guidance, sequencing, and insertion parameters. The three-sigma envelope of thrust, flow rate, liftoff mass, and wind speed variations is given, along with impact data, in the Range Safety part of this report. A study of wind disturbances, three-sigma C_1 and C_2 variations, and + 10%control gain deviations shows the vehicle to be structurally capable of withstanding the expected winds during the launch period. Pertinent tracking and telemetry ground coverage data are presented for poweled Buthon and orbital flight phases.

NASA-GEORGE C. MARSHALL SPACE FLIGHT CENTER

TECHNICAL MEMORANDUM X-53293

July 13, 1965

SA-10 FLIGHT MECHANICAL SUMMARY

FLIGHT MECHANICS BRANCH
OPERATION STUDIES BRANCH
FLIGHT EVALUATION AND OPERATIONS STUDIES DIVISION
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SUMMARY

The trajectory for SA-10 is shaped to insert the S-IV stage/Pegasus C combination into a circular orbit at approximately 535 km altitude, measured at insertion. The predicted nominal orbital lifetime is 725 days. The probabilities of achieving guidance cutoff and of not permitting the LH₂ residuals to exceed 250 lbm have been equalized at a value of 95.5%.

The pitch program for the S-I stage is identical to that of SA-8 and essentially provides a minimum angle of attack through the high dynamic pressure region. The Iterative Guidance Mode (IGM) is employed to guide the S-IV stage in pitch, with a delta minimum guidance mode in cross range.

The S-I booster will propel the vehicle to an altitude of 88.94 km and range of 79.70 km. After separation of the S-I and S-IV stages, and approximately 2 seconds of ullage rocket operation, S-IV mainstage ignition occurs. The S-IV main engines burn continuously until the guidance computer initiates the Guidance Cutoff Signal (GCS), which will occur when the inertial velocity reaches 7592 m/s. After 10 seconds elapse to permit complete thrust decay, orbital insertion will occur at 642.085 seconds after liftoff.

The vehicle wind limit is no less than 65 m/s from any azimuth and is more than twice the three sigma maximum wind for the predicted month of launch. The fueled vehicle free standing and launch release surface wind limits are 16.9 and 10.3 m/s, respectively.

A 95.5% confidence level exists of not exceeding roll and tumble rates of 9 deg/sec and 2 deg/sec, respectively.

PART I TRAJECTORY

A. INTRODUCTION

The Block II vehicle SA-10, consisting of two live stages, Instrument Unit, Apollo Boilerplate, and Pegasus Payload (Figure I, 1 & 2), is scheduled to ascend from Launch Complex 37B, Eastern Test Range Facilities in the summer of 1965. SA-10 will have a launch azimuth of 90 degrees East-of-North, and will roll into a 95.2 degree East-of-North flight azimuth.

This trajectory is based on propulsion (References 1 and 2) and mass (Reference 3) data provided by P&VE Laboratory. The first stage will be propelled by eight Rocketdyne H-l engines providing a total thrust of 1.5 million pounds. Six 15,000 pound thrust, Pratt & Whitney, RL10A-3 engines power the S-IV stage during flight. The S-I stage measure 6.5 meters in diameter and 24.5 meters in length. The S-IV stage is basically a 5.6 meter-diameter cylinder measuring 12.5 meters in length. With the Instrument Unit, Payload and Launch Escape System (LES), the total vehicle configuration stands approximately 57.3 meters and has a liftoff mass of 511,709 kg (1,128,124 lbm). Found in Reference 4 is a more complete description of the vehicle and payload. There will be no onboard camera coverage of separation, and likewise, no television monitoring of Pegasus deployment.

B. DESCRIPTION

The SA-10 vehicle will lift off from Pad 37B, rising vertically for 9 seconds in order to clear the launch facilities and then simultaneously begin its pitch program and roll maneuver. The roll rate will be nominally one degree per second.

The first stage trajectory was shaped to minimize aerodynamic moments during the period of highest dynamic pressure. The tilt program is not biased for wind as the launch date occurs during a low wind period. The entire flight program was optimized to attain the maximum performance while achieving the desired orbital mission objectives which, briefly, are:

- 1. Provide a near-circular orbit in the region of 500 km altitude (270 nautical miles) at the end of one year.
- 2. Insert into an orbit having an inclination of approximately 28.87 degrees.
 - 3. Maximize guidance cutoff probability.
 - 4. Minimize residual LH2 at guidance cutoff.

A tilt arrest of 52.45 degrees is programmed at 138 seconds after liftoff to insure ample damping time for various sloshing and transient motions in order to avoid premature cutoff and separation sequences. The separation sequence of events is commanded from a timer which is initiated by propellant level sensors (Reference 5).

After separation, tilt arrest is continued until 168 seconds after liftoff, allowing sufficient time for the LES tower and ullage casings to be jettisoned. The Launch Escape System has only one active motor, the jettison motor. This motor provides the capability of separating the LES from the Command Module (CM) during an abort mode or during normal flight.

The Saturn guidance system, Iterative Guidance Mode (IGM), implemented approximately 18 seconds after separation, will guide the S-IV vehicle to the desired terminal conditions. Guidance Cutoff Signal (GCS) is sent by the onboard computer (ASC-15) when the inertial velocity reaches 7592.0 m/s.

B. DESCRIPTION (CONT.)

Orbital insertion is defined to occur 10 seconds after the Guidance Cutoff Signal is generated by the guidance computer. Upon GCS the S-IV stage undergoes a 180-second duration non-propulsive venting period to reduce residual hydrogen in the tank. At the end of this period the vents close followed one second later by separation of the Apollo boilerplate from the Pegasus C/S-IV stage combination. The Pegasus satellite will begin its wind deployment 60 seconds after Apollo boilerplate separation, requiring approximately 60 seconds for this function.

C. RESULTS

The orbital mission objectives are achieved to the following degree:

- 1. The nominal orbital altitude after one year is 500 km. An orbital altitude history for nominal and minus three-sigma atmospheric conditions is presented in Figure I-3.
- 2. The nominal inclination of the osculating conic at the time of insertion is 28.88 degrees.
 - 3. The probability of a guidance cutoff is 95.5%.
- 4. The probability of LH_2 residuals not exceeding 250 lbm is 95.5%.

A summary of the SA-10 vehicle characteristics, trajectory history and insertion and orbital conditions is presented in Table I-I. Predicted vehicle characteristics to be used for post-flight evaluation are presented in Table I-II. The S-I stage pitch steering program, the S-IV guidance terminal conditions and the vehicle sequence of events are detailed in Tables I-III, -IV, and -V, respectively. A brief mass characteristics outline is presented in Table I-VI. The powered flight trajectory from liftoff to Pegasus/Apollo boilerplate separation and the S-I stage retro and coast-to-impact trajectory are presented in detail in Table I-VII, A through J.

The flight profile is graphically presented in Figure I-4 with its nominal pitch steering program presented in Figure I-5.

The earliest S-I inboard engine failure which still results in guidance cutoff is 90 seconds after liftoff. An outboard failure will not permit a guidance cutoff, but failure after 140 seconds from liftoff will result in an orbit with perigee greater than 400 km altitude.

Table I-I SA-10 FLIGHT DATA

(All values are inertial where applicable unless otherwise denoted.)

A. LAUNCH & TRAJECTORY DATA

Launch Complex and Pad	37В
Latitude at Launch (Geodetic)	28.53185 degrees (N)
Longitude at Launch	80.56495 degrees (W)
Launch Azimuth	90° E of N
Flight Azimuth	95.2° E of N
S-I Stage Roll Angle	5.2 degrees
S-I Stage Mach One	55 seconds
S-I Stage Maximum Dynamic Pressure	67 seconds
S-I Stage Pitch Angle at Tilt Arrest	52.45 degrees
S-I Stage Velocity at OECO (Inertially Ref) (Earth Ref)	3051.17 m/s 2714.87 m/s
S-I Stage Path Angle at OECO (Inertially Ref) (Earth Ref)	56.810 degrees 52.032 degrees
S-I Stage Altitude at OECO	88.94 km
S-I Stage Range at OECO	79.70 km
S-IV Stage Guidance Cutoff Signal (GCS)	632.085 sec
S-IV Stage Velocity at GCS	7592.00 m/s
S-IV Stage Path Angle at GCS	89.994 degrees
S-IV Stage Altitude at GCS	535.754 km
S-IV Range at GCS	1844.208 km
S-IV Stage Latitude at GCS (Geocentric) S-IV Stage Longitude at GCS	25.270 degrees 62.297 degrees (West)
. INSERTION CONDITIONS	
Insertion Time	642.085 seconds
Velocity	7595.0 m/s
Path Angle (against local vertical)	90.0008 degrees
Altitude (oblate earth)	535.708 km

В.

SA-10 FLIGHT DATA (CONT.)

	Range	1910.20 km
	Latitude (Geocentric)	25.111 degrees
	Longitude	61.665 degrees (West)
	Azimuth	104.759 degrees
c.	ORBITAL CHARACTERISTICS (spherical earth; R_e = 6,378.165 km)	
	Perigee Altitude	531.6 km
	Apogee Altitude	531.9 km
	Anomalistic Period	95.27 min
	Semi-Major Axis	6909.9 km
	Eccentricity	.00002
	Inclination	28.88 degrees
	Longitude of Ascending Node	176.5 degrees (East)
	Argument of Perigee	258.5 degrees
	True anomaly at Insertion	220.0246 degrees
	Eccentric Anomaly at Insertion	220.0254 degrees
	Mean Anomaly at Insertion	220.0261 degrees
	Regression Rate of Node	-6.6 deg/day
	Rate of Change of Argument of Perigee	+10.7 deg/day
	Vis Viva Energy (Twice Total Energy)	$-57.77 \mathrm{Km}^2/\mathrm{sec}^2$
	Nominal Lifetime	725 days
	-3σ Lifetime	532 days
	Ballistic Parameters for Tumbling Vehicle $\mathbf{C}_{D}\mathbf{A}$	265 m ²
	Post Venting Orbital Mass	10323 kgs
	Ballistic Coefficient CDA/m	.026 m ² /kg

TABLE I-II

PREDICTED VEHICLE CHARACTERISTICS FOR FLIGHT EVALUATION COMPARISON

S-I Stage

The S-I thrust averages are obtained by considering the longitudinal components of thrust, reduced to sea level throughout flight. They are as follows:

$$F_T = F_1 + F_2$$

where F_1 is the main engine thrust average and F_2 is the turbine exhaust thrust average.

 $F_1 = 6,776,786 \text{ newtons} (1,523,482 \text{ 1bf})$

 $F_2 = 13,732 \text{ newtons}$ (3,087 1bf)

 $F_{T} = 6,790,518 \text{ newtons} (1,526,569 \text{ 1bf})$

The S-I_flow rate is derived as follows:

$$\dot{W} = \begin{bmatrix} W(T=0) & -W(T=140) & -W \\ & & & \end{bmatrix} / 140 ,$$

where W_{aux} = Ice, trapped environment, and chilldown.

:. $\dot{W}_T = 2682 \text{ kg/sec } (5913.5 \text{ lbs/sec})$

 $I_{sp} = 258.1 \text{ sec}$

S-IV Stage

The S-IV stage thrust averages are vacuum values averaged from 1.8 second to 480.0 seconds of S-IV flight time.

$$F_T = F_1 + F_2 + F_3$$

TABLE I-II (continued)

where F_1 is the engine thrust along longitudinal axis = 397486 newtons (89358 lbf)

 F_2 = Thrust due to cluster effect = -2785 newtons (-626 lbf)

 F_3 = Helium heater and leakage thrust through chilldown ducts = 734 newtons (165 lbf)

 $F_T = 395,435$ newtons (88,897 lbf).

The flow rate is also obtained from 1.8 seconds to 480.0 seconds of S-IV flight time.

 \dot{W}_{T} = 95 kg/sec (208.8 lbs/sec)

 $I_{sp} = 425.8 \text{ sec}$

TABLE 1-III

PITCH TILT PROGRAM FOR SATURN I VEHICLE SA-10

Flight Time (sec)	(deg)	Flight Time (sec)	(deg)	Flight Time (sec)	(deg)
0	0	33	6.70	66	24.65
1	0	34	7.15	67	25.25
2	0	35	7.65	68	25.80
3	0	36	8.10	69	26.35
4	Ö	37	8.60	70	26.95
5	Ö	38	9.10	71	27.50
6	Ö	39	9.60	72	28.10
7	0	40	10.10	73	28.65
8	0	41	10.65	74	29.15
9	0	42	11.10	75	29.75
10	0.25	43	11.70	76	30.30
11	0.30	44	12.25	77	30.80
12	0.45	45	12.80	78	31.40
13	0.60	46	13.30	79	31.90
14	0.65	47	13.90	80	32.45
15	0.90	48	14.40	81	33.00
16	1.05	49	14.90	82	33.50
17	1.25	50	15.50	83 ⁻	34.05
18	1.45	51	16.10	84	34.50
19	1.70	52	16.60	85	35.00
20	1.95	53	17.15	86	35.50
21	2.25	54	17.75	87	36.00
22	2.50	55	18.30	88	36.45
23	2.85	56	18.85	89	36.90
24	3.20	57	19.45	90	37.40
25	3.50	58	20.00	91	37.85
26	3.85	59	20.60	92	38.25
27	4.25	60	21.20	93	38.75
28	4.60	61	21.75	94	39.15
29	5.00	62	22.35	95	39.65
30	5.45	63	22.90	96	40.00
31	5.85	64	23.50	97	40.40
32	6.25	65	24.05	98	40.85

TABLE I-III (CONT)

Flight Time (sec)	(deg)	Flight Time (sec)	(deg)
99	41.20	134	51.75
100	41.65	135	51.75
101	42.00	136	52.15
102	42.35	137	52.40
103	42.80	138	52.45
104	43.15	*168	52.45
105	43.50		
106	43.85		
107	44.25	j	
108	44.60		
109	44.90		
110	45.25		
111	45.55		
112	45.90		
113	46.25		
114	46.50		
115	46.85		
116	47.15	1	
117	47.50	ļ.	
118	47.70		
119	48.05		
120	48.35		
121	48.60		
122	48.85		
123	49.10		
124	49.40	\	
125	49.65	Į.	
126	49.90		
127	50.15	1	
128	50.40		
129	50.60	1	
130	50.85		
131	51.10		
132	51.30		
133	51.50		

*Time of IGM

TABLE I-IV IGM TERMINAL CONDITIONS

The following defines the necessary IGM terminal conditions.

```
\eta_T = Terminal Radius Vector

\dot{\eta}_T = Terminal Time Rate Change of \eta_T

\dot{\xi}_T = Terminal Tangential Velocity

\dot{V}_T = Terminal Total Velocity = \sqrt{\dot{\eta}_T^2 + \dot{\xi}_T^2})

\dot{\eta}_{gT} = Terminal Radial Acceleration Due to Gravity

\dot{\xi}_{gT} = Terminal Tangential Acceleration Due to Gravity

\dot{\xi}_{gT} = Time-To-Go (initially)

\dot{V}_{ex} = Exhaust Velocity (g_0 \cdot I_{sp})
```

The values for the above for SA-10 are as follows:

TABLE I-V
SA-10 SEQUENCE OF EVENTS

TIME (From Liftoff)	EVENT
0.0	Liftoff
9.0	Initiate Roll and Pitch Tilt
14.2	Terminate Roll
137.7	Signal from Sequencer to Enable Level Sensors
138.0	Tilt Arrest
141.7	S-I Stage Level Sensor Signal
143.52	Inboard Cutoff (S-I Stage)
149.52	Outboard Cutoff (S-I Stage)
150.22	Ullage Rocket Ignition (S-IV Stage)
150.32	Separation, Immediately Followed by Retro Rocket Ignition (S-I Stage)
152.02	S-IV Mainstage Ignition
154.02	Ullage Rocket Thrust Termination
162.32	Jettison Ullage Rocket Casing and LES
168.00	Initiate Active Guidance
595.00	Signal from Sequencer to Arm LOX Cutoff Capability
632.085	S-IV Stage Guidance Cutoff Signal
642.085	End of Powered Flight
812.085	Close Blowdown Non-Propellant Vents
813.085	Start S-IV Pegasus/Apollo Separation
873.085	Begin Pegasus Wing Deployment
933.085	Terminate Wing Deployment

TABLE I-VI
SA-10 Mass Characteristics

Total Mass at Liftoff	511,709 kg	(1,128,124 1bm)
Mass at First Stage Cutoff (OECO)	117,035 kg	(258,018 1bm)
Mainstage Consumption During First Stage of Flight (To Separation)	392,332 kg	(864,943 1bm)
Mass at Second Stage Ignition (152.02 sec)	62,339 kg	(137,435 1bm)
Mass at Second Stage Cutoff (632.09 sec)	15,527 kg	(34,230 lbm)
Mainstage Consumption During Second Stage of Flight	45,315 kg	(99,903 1bm)
Flight Performance Reserve at S-IV Cutoff	341 kg LOX 48 kg LH ₂	•
Orbiting Payload	10,323 kg	(22,758 1bm)

I-VII-A	
TABLE	,

						TABLE I-1	I-VII-A				
						S-I STAGE NOMINAL TRAJECTORY	TRAJECTORY				
	TIME	GROUND DISTANCE	ALTITUDE	SPACE FIXED	SPACE FIXED PATH ANGLE	ACCELERATION V DOT	MASS	DYNAMIC PRESSURE	THRUST	MACH	DRAG
	(SEC)	(KM)	(KM)	2 S	(DEG)	EARTH-FIXED (M/SEC SQ)	(KG)	(DS M/N)	Š		Z
	•	•	•	08.	90.00	00.0-	511709	o	591447	00.00	44130
	5.0	00.0-	0.07	409.3	7.	•	984	173	6729211	0.05	21561
	ċ	0	.2	10.	4.9	0	85	172	6746657	0.11	43611
	'n	•	4.	13.	1.9	4.52	7174	1904	6808281	0.17	69583
	ċ	়	۲.	18.	8.7	6.	.0	3669	6864335	0.24	99172
	Š	0	• 2	27.	5.4	4.	490	6119	38	0.32	133807
	•	•	8	40,	2.0	6.02	431453	9250	6978002	0.40	177049
	5		•	59.	8.6		96	12988	7045927	0.50	235500
	•	0.25	3	83.	65.55	7.19	1440	17171	7118720	0.61	306280
	Š	4.	•	13.	\sim	7.76	9606	21559	7193932	0.73	417967
	ċ	. 7	6.	46.	0	8.21	46	25740	7268606	0.86	595333
	δ.	7	6	88.	ထာ	8.12	6392	29117	7337010	1.01	983131
	ċ	•	8.9	31.	-	8.81	u١	31255	7398730	1.17	1091850
	Š.	٠,	0.7	80.	•	10.00	4.1	32486	7458789	1.36	•
	•	?	2.7	37.	۷n	11.52	rv	32432	7514121	1.58	942661
	Š.	ن .	4.9	03	4	13,30	_	30424	7566491	1.83	785143
	· •	•	7.4	79.	4	15.25	ഗ	26312	7609216	5.09	614399
	ŝ	4.	0.1	965.	J	17.32	w	21043	7641497	2.33	447029
	•	4.6	3.0	062.		19.39	w	16359	7660389	2.60	313563
	95.	1.8	6.3	169.	m	21.48	u ı	12323	7668134	2.91	213636
	•		6.	86.	53.99	23.65	242198	8913	11699	3.23	137667
	02	8.1	3.9	415.	•	25.91	·N	6155	99	3.57	84429
	9	2.1	8.2	554.	J	28.30	215307	4086	65947	3.92	51775
	15.	9.9	3.0	706.	√T	30.87	201895	5629	2	4.29	31156
	20.	1.9	8.1	872.	EU.	33.74	188484	1660	63458	4.70	18507
	25.	7.8	3.7	052.	Ln.	36.98	175122	1053	7623263	5.31	9112
	30.	4.6	9.8	249.	S	40.66	161761	625	7607077	6.10	2985
	35.	2.2	6.4	466.	S.	44.89	148468	330	7586496	7.07	746
	40.	0.7	3.6	705.	O	_	35	148	7563821	8.24	55
Ξ	43.	4.4	9.1	890.	vo	9	~	74	54	9.22	9
	45	6.0	1.5	937.	vo.	0	122997	52	88540	9.55	54
(2)	49.	9.7	8 6	051.	6.8	2	703	15	4355	10.08	21
	•	0.7	9.7	057.	9	-3.25		13	301796	10.10	18
3	ċ	1.4	0.2	056.	6.8	Ś	116248	12	7042	10.01	16

⁽¹⁾ IECO (2) OECO (3) Separation

^{3 8}

222E (KM)

YYYE (XX)

XXXE (XX)

TIME SEC)

EARTH FI	EARTH FIXED PARAMETERS	TERS		1	LONGITUDE	GEOD. LAT.	GEOC. LAT.
DXXE	DYYE	DZZE	VELOCITY	ANGLE	WEST)	NOR TH)	NORTH
(M/SEC)	(M/SEC)	(M/SEC)	(M/SEC)	(DEC)	(DĒG)	(DEG)	(DEG)
0.0	0.0	0.0	0.0	00.00	80.5650	28.5319	28.3707
0.0-	17.1	0.0-	17.1	0.21	80.5650	28.5319	28.3707
-0-1	36.4	0.0-	36.4	0.25	80.5650	28.5319	28.3707
0.3	57.9	0.0-	57.9	0.33	80.5650	28.5319	28.3707
1.7	81.6	0.0-	81.6	1.17	80.5649	28.5319	28.3707
4.7	107.7	0.0-	107.8	2.51	80.5648	28.5319	28.3707
10.2	136.2	0.0-	136.6	4.29	80.5644	28.5319	28.3707
18.8	167.0	0.0	168.1	6.42	80.5637	28.5318	28.3706
31.1	200.1	0.0	202.5	8.82	80.5624	28.5317	28.3706
47.5	235.2	0.1	240.0	11.39	80.5604	28.5316	28.3704
68.2	271.5	0.1	280.0	14.09	80.5575	28.5314	28.3702
93.1	307.4	0.2	321.2	16.82	80.5534	28.5311	28.3699
122.0	342.0	0•3	363.1	19.60	80.5480	28.5307	28.3695
156.8	378.8	0.5	410.0	22.45	80.5409	28.5302	28.3690
198.4	419.1	9*0	463.7	25.28	80.5320	28.5295	28.3683
247.7	463.6	0.8	525.6	28.06	80.5207	28.5286	28.36,74
305.6	512.8	1.1	597.0	30.72	80.5067	28.5275	28.3663
372.7	566.8	1.4	678.4	33.24	80.4896	28.5261	28.3649
449.5	625.3	1.7	770.2	35.61	80.4688	28.5244	28.3633
536.2	688.1	2.2	872.3	37.80	80.4440	28.5224	æ
635.9	154.9	5.6	985.1	39.83	80.4145	28.5200	28.3588
739.9	826.0	3.2	1109.0	41.67	80.3799	28.5171	28.3560
857.7	901.6	3.9	1244.4	43.36	80.3397	28.5138	28.3527
6.986	981.9	4.5	1392.2	44.89	80.2934	28.5099	28.3488
1128.6	1067.7	5.3	1553.6	46.29	80.2403	28.5054	28.3443
1284.1	1159.6	6.1	1730.2	47.56	80.1798	28.5003	28.3392
1455.1	1258.9	7.1	1924.1	48.72	80.1113	28.4944	28.3334
1643.5	1367.0	8.2	2137.7	49.76	80.0339	28.4877	28.3267
1851.8	1486.0	9. 4	2374.3	69.05	79.9468	28.4802	28.3192
2011.2	1579.0	10.4	2557.0	51.24	79.8792	28.4742	28.3132
2053.9	1599.2	10.7	2603.1	51.45	79.8492	28.4716	28.3106
2161.4	1642.8	12.0	27,14.9	52.03	79.7546	28.4631	28.3022
2168.1	1643.6	12.1	2720.7	52.09	79.7439		28.3013
2168.6	1641.3	12.1	2719.7	52.13	79.7374	28.4616	28.3007

0.0 1

149.5 150.0 150.3

(2) 3 Separation

IECO OECO 36E

		DRAG	2	100 80 57
		MACH		10.07 9.97 9.81
		THRUST	(X)	62517 62517 62517
	RY	DYNAMIC PRESSURE	(N/M SQ)	12 9
2	ON TRAJECTO	MASS	(KG)	62419 62387 62339
OLITALT STORT	S-IV ULLAGE PORTION TRAJECTORY	ACCELERATION V DOT	EARTH-FIXED (M/SEC SQ)	-4.84 -4.83 -4.80
		SPACE FIXED PATH ANGLE	(066)	56.89 56.98 57.11
		SPACE	(M/SEC)	3056.4 3053.6 3049.3
	,	ALTITUDE	(X X)	90.28 91.41 93.10
		GROUND DISTANCE	(KM)	81.40 82.83 84.99
		TIME	(SEC)	150.3 151.0 152.0

	GEOC. LAT.	NORTH)	28.3007 28.2994 28.2974
	GEOD. LAT.	NORTH)	28.4616 28.4603 28.4583
	LONGITUDE	MEST) (DEG)	79.7374 79.7228 79.7009
	РАТН	ANGLE (DEG)	52.13 52.22 52.36
TRA.TECTORY		VELOCITY (M/SEC)	2719.7 2716.4 2711.5
TABLE I-VII-D	TERS	DZZE (M/SEC)	12.1 12.3 12.4
TAB	EARTH FIXED PARAMETERS	DYYE (M/SEC)	1641.3 1635.4 1626.6
	EARTH FI	DXXE (M/SEC)	2168.6 2168.9 2169.4
		222E (KM)	000
		YYYE (KM)	89.8 90.9 92.5
		XXXE (KM)	82.6 84.0 86.3
18		TIME (SEC)	150.3 151.0 152.0

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	DRAG	Ŝ	57	45	m	6	-	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	MACH		ဆ	79.6	3	.2	.2	٦.	8	•2	6.	8		•	•	•	•	• 6	•	•	•.	•	•	•	۲.	3.76	ဆ	æ	6.	6•	•	0	7	.2	4.33	4.41	4.51	4.60	۲.	4.82	4.93	•
	THRUST	(2)	63320	261	54	S	537	72	233	0112	0002	9866	9971	9922	9883	9807	9716	9639	9578	9536	9520	9508	9509	9515	9503	394763	9445	9417	9395	9395	9400	9421	9427	9456	9410	9390	9370	9358	5	9354	-	9382
	DYNAMIC PRESSURE	(N/M SQ)	-	S	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
TRA.TECTORY	MASS	(KG)	233	62301	145	865	943	894	798	702	90	510	414	318	222	126	031	936	841	47	652	558	G	369	74	-	9	991	897	803	709	615	521	427	332	238	144	050	926	862	16	674
S-TV STAGE NOWTNAT.	ACCELERATION V DOT	EARTH-FIXED (M/SEC SQ)		4.	•	.2	.		•	9	6.	7	3	8	7	£.		6•	• 5	ż	6.		.5	6.	٠,		•	e.	•	•	4.	æ	• 2	. 7	٦.	0.5	1.0	3	2.0		7	•
	SPACE FIXED Path angle	(DEG)	7.1	57.23	8.2	8.3	8.9	9.4	0.3		61.99	~	. ^		2	0	66.85	7.6	8.4	9.2	6.6	0.7	71.46	2.2	Q.	3.6	74.34	0.0	5.7	4	\circ	17.72	3	79.01	9.6	80.25	0.8	1.4	2.0		3.2	3.7
	SPACE FIXED	VELUCIIY (M/SEC)	049.	045.	056.	058.	067.	076.	.460	114.	136.	161.	189.	219.	252.	288.	327.	369.	413.	460.	511.	564.	621.	681.	744.		881.	954.	031.	112.	196.	284.	377.	473.	574.	679.	788.	902.	021.	145.	274.	4 09.
	ALTITUDE	(KM)	3.1	4.7	8.60	10.9	18.9	26.7	42.2	57.4	72.2	86.8	01.1	15.1	28.9	45.4	55.6	68.5	81.2	93.6	2250	17.6	29.3	40.6	51.7	362.64	73.2	83.5	93.6	03.4	12.9	22.1	31.1	39.7	48.1	56.1	63.9	71.3	78.4	5.2	91.6	91.6
	GROUND DISTANCE	(KA)	6.4	87.07	6.90	08.3	19.2	30.1	52.1	74.5	97.2	20.3	43.8	67.6	91.8	16.5	41.6	67.2	93.3	19.8	47.0	74.7	05.9	31.8	61.4	591.59	22.4	54.0	86.4	19.5	53.4	88.2	23.8	4.09	97.9	36.3	75.8	16.3	058.0	7.00	144.7	189.9
	TIME	(SEC)	52.	53.	62.	63.	68.	73.	83.	93.	03.	13.	23.	33.	43.	53.	63.	73.	83.	93.	03.	13.	23.	33.	43.	353.0	63.	73.	83.	93.	03.	13.	23.	33.	43.	53.	63.	73.	83.	93.	03.	13.

	DRAG	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	MACH		5.18	5.32	5.46	5.61	5.78	5.94	6.12	6.31	6.51	6.72	6.94	7.16	7.16	7.16	7.17	7.17	7.17	7.17
	THRUST	Ĉ.	394048	394280	394498	394649	394684	394685	394645	394,505	394339	394278	394403	396449	11947	0	0	0	0	0
AT.) SCTORY	DYNAMIC PRESSURE	(N/M SQ)	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
TABLE I-VII-E (CONT TAGE NOMINAL TRAJEC	MASS	(KG)	25807	24866	23924	22981	22038	21095	20152	19209	18267	17325	16383	15527	15506	15497	15383	10787	10765	10323
TABLE I-VII-E (CONT) S-IV STAGE NOMINAL TRAJECTORY	ACCELERATION V DOT	EARTH-FIXED (M/SEC SQ)	14.30	14.94	15.63	16.36	17.13	17.95	18.84	19.79	20.81	21.94	23.22	24.68	0.75	0.01	.01	.01	.01	.01
	SPACE FIXED PATH ANGLE	(DEG)	84.32	84.86	85.40	85.93	86.45	86.97	87.48	88.00	88.51	89.02	89.53	89.99	90.00	00.06	90.01	90.01	90.01	90.01
	SPACE FIXED	VELOCITY (M/SEC)	5549.7	5696.6	5850.1	9.0109	6178.6	6354.4	6538.6	6732.0	6935.1	7149.0	7374.6	7592.0	7594.4	7595.0	7595.5	7595.5	7595.5	7596.0
	ALTITUDE	χ Σ	503.30	508.57	513.43	517.88	521.90	525.46	528.54	531.12	533.16	534.64	535.52	535.75	535.75	535.71	534.75	534.74	534.51	533.92
	GROUND DISTANCE	(KM)	1236.37	1284.17	1333,35	1383,99	1436.14	1489.88	1545.28	1602.42	1661.39	1722.28	1785.19	1844.21	1850.81	1910.20	3032,34	3038,95	3435.08	3831.25
	TIME	(SEC)	523.0	533.0	543.0	553.0	563.0	573.0	583.0	593.0	603.0	613.0	623.0	(2) 632.1	633.1	(3) 642.1	(4) 812.1	(5) 813.1		

Initiate Active Guidance
 GCS
 Insertion
 Close LH2, non-propulsive vent valves
 Pegasus/Apollo boilerplate separation
 Begin wing deployment
 Terminate Wing deployment

TABLE I-VII-F S-IV STAGE NOMINAL TRAJECTORY

GEOC	EG)	8.297	8.295	8.277	8.275	8.265	8.255	8.233	8.211		8.162	8.137	8.110	8.082	8.053	8.023	7.992	7.960	7.926	7.891	7.854	7.816	7.777	7.735	7.692	7.648	7.601	7.552	7.501	7.448	7.393	7.335	7.275	7.212	7.146	7.077	7.005	6.930	5.851	6.769	5.683
GEOD.	US1-17 NORTH) (DEG)	8.458	8.456	8.438	8.436	8.426	8.416	8.394	8.371		8.323	8.297	8.270	8.242	8.213	8.183	8.152	8.119	8.085	8.050	8.014	7.975	7.936	7.894	7.851	7.806	7.759	7.710	7 • 659	7.606	7.551	7.493	7.432	7.369	7.303	7.234	7.161	7.086	7.007	5.924	5.837
LONGITU	(PUSI-1VE WEST) (DEG)	9.700	9.679	9.478	9.463	9.353	9.242	9.018	8.791	78.5617	8.328	8.090	7.850	7.605	7.355	7.102	6.844	6.581	6.313	6.040	5.761	5.477	5.187	4.891	4.588	4.279	3.962	3.639	3.308	2.969	2.623	2.268	1.905	1.532	1.151	0.759	0.358	9.947	9.525	9.092	8.648
; + •	ANGLE (DEG)	2.3	2.4	3.6	3.7	4.4	5.0	9.0	6.9	57.93	ж Ж	ж 6.	0.1	1.7	2.6	3.6	4.5	5.4	6.3	7.2	8.1	0.6	6.6	0.7	1.6	2.4	3.2	•	æ.	5.6	6.3	7.1	7.8	8.5	9.2	6.6	9.0	1.2	1.9	2.5	3.2
	VELOCITY (M/SEC)	711.	707.	713.	713.	7.20.	726.	740.	756.	4	795.	819.	845.	875.	907.	943.	981.	022.	.990	114.	164.	218.	275.	336.	4 00	468.	539.	614.	663.	775.	862.	952.	047.	146.	250.	358.	471.	588.	7111.	39.	973.
ETERS	D22E (M/SEC)	2.	2	4	4	•	•	-	•	28.3	_	.	•	6	_:	.	9	6	;	4	-	ċ	3.	•	•	3	•	•	•	œ	2	96	Ϊ.	05.	10.	.	19.	•	30.	ŝ	41.
IXED PARAME	DYYE (M/SEC)	26.	18.	•69	65.	541.	17.	476.	37.	399	360.	21.	282.	243.	204.	164.	123.	82.	40.	98.	54.	.60	64.	17.	68.	18.	67.	13	2	00	39	17.	11:	43.	71.	•	-	65.	3	44.	340
EARTH FI	DXXE (M/SEC)	169.	170.	213.	216.	241.	265.	309.	351.	'n.	44 I •	490	540.	592.	646.	702.	760.	821.	884.	646	016.	086.	159.	234.	311.	392.	475.	561.	649	741.	835.	933.	034.	138.	245.	355.	469.	586.	707.	831.	960.
	222E (KM)	•	•	•	•	•	•	•	•	7.	٠	•	•	•	•	•	٠	•		٠	٠	٠	•	٠	•	6	•	•		7	'n	4	Š	•	-	æ	6	-	2	3	Š
	YYYE (KM)	2.	94.	60	10	17.	25.	• • •	52	169.2	20	96	60	22.	34.	46.	57.	68	6.	89.	•66	08	17.	25.	33.	41.	48	54.	9,	65	0.	14.	7.7	80	82.	84.	84.	84.	83.	81.	78
	XXXE (KM)	•	88	80	0.	21.	32.	50.	.87	202.6	97		9	02.	ς 2.	55.	82.	0	39.	68.	98	28.	59.	91.	24.	57.	92.	27.	500	200	38	77	17.	27.	999.	42.	086.	132.	178.	226.	275.
	TIME (SEC)	52.	53.	62.	63.	68	73	83	93	203.0	13.	, ç		43	5	63	73.		93	03.	13.	23.	33.	43.	53.	63	5	9 0	, C	500	13.	23.	33	43.	53.	63.	73.	63	93.	03.	13.

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TABLE I-VII-F (CONT.)

	2					NI-S	STAGE NOMI	S-IV STAGE NOMINAL TRAJECTORY				
					EARTH FI	FIXED PARAMETERS	TERS			LONG I TUDE	GEDD. LAT.	GEDC. LAT
									PATH	(POSITIVE	(POSITIVE	(POSITIVE
	TIME	XXXE	YYYE	222E	DXXE	DYYE	D22E	VELOCITY	ANGLE	WEST)	NOR TH.	NORTH)
	(SEC)		(X X)	(X X)	(M/SEC)	(M/SEC)	(M/SEC)	(M/SEC)	(DEC)	(DEC)	(0EG)	(DEG)
	523.0		374.4	26.5	5092.3	-442.6	146.8	5113.6	83.83	68,1921	26.7473	26.5929
	533.0		369.5	28.0	5228.7	-549.6	152.7	5259.7	84.43	67.7236	26.6524	26.4984
	543.0		363.4	59.6	5369.5	-662.6	158.8	5412.6	85.03	67.2423	26.5529	26.3994
	553.0		356.2	31.2	5514.8	-782.1	165.1	5572.5	85.61	66.7477	26.4487	26.2955
	563.0		347.8	32.9	5664.9	-908.7	171.6	5739.9	86.18	66.2393	26.3394	26.1867
	573.0		338.0	34.6	5819.8	-1043.1	178.3	5915.2	86.74	65.7165	26.2247	26.0725
	583.0		326.9	36.4	5979.8	-1185.9	185.2	6099.1	87.30	65.1786	26.1043	25.9526
	593.0		314.3	38•3	6145.2	-1338.1	192.3	6292.2	87.85	64.6251	25.9780	25.8267
	603.0		300.1	40.3	6316.2	-1500.7	199.6	6495.1	88.40	64.0551	25.8452	25.6945
	613.0		284.2	42.3	6493.0	-1674.7	207.2	6708.7	88.95	63.4680	25.7055	25.5555
	623.0		266.5	44.4	4.9199	-1861.3	215.0	6934.3	89.50	62.8628	25.5586	25.4092
(5)	632.1		248.8	46.4	6850.3	-2042.1	222.3	7151.7	89.99	62.2966	25.4185	25.2696
	633.1		246.8	46.6	6850.3	-2050.5	222.7	7154.1	90.06	62.2334	25.4027	25.2539
(3)	642.1		228.0	48.6	6831.3	-2114.7	226.3	7154.7	90.00	61.6650	25.2589	25.1107
(4)	812.1		-231.7	92.3	6353.5	-3280.3	6,787	7156 0	90.01	51 2061	1007	1000
(2)	813.1		-235.0	92.6	6350.1	-3286.9	285.2	7156.0	90.01	51 1/61	22.1034	21.9695
(9)	873.1		-444.0	110.2	6133.1	-3675.7	301.4	7156 5	10.00	77.50%	22.0825	21.9488
3	933.1	3905.0	-675.8	128.7	5892.3	-4050.4	315.0	7157.1	90.01	44.0888	19,4052	20.6581 19 2850
										1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1	0.004

Initiate Active Guidance
 GCS
 Insertion
 Close LH2 non-propellant vent valves
 Pegasus/Apollo boilerplate separation
 Begin Wing deployment
 Terminate Wing deployment

MARSHALL SPACE FLIGHT CENTER

S-I RETRO PORTION TRAJECTORY TABLE I-VII-G

DRAG	2	1828 1453 1306 942 816
МАСН		10.07 9.95 9.89 9.70 9.62
THRUST	ŝ	275724 406239 468726 587092
DYNAM IC PRESSURE	(N/M SQ)	12 9 8 6 5
MASS	(KG)	53929 53663 53537 53194 53117
ACCELERATION V DOT	EARTH-FIXED (M/SEC SQ)	-10.99 -13.42 -14.60 -16.85 -5.80
SPACE FIXED Path angle	(DEG)	56.89 56.99 57.04 57.18
S PACE F IXED	VEL BC I TY (M/SEC)	3056.4 3048.6 3044.3 3028.9 3023.2
ALTITUDE	(KM)	90.28 91.41 91.94 93.59 94.32
GRØUND / DISTANCE	χ Σ	150.3 81.40 151.0 82.83 151.3 83.51 152.3 85.62 152.8 86.56 (1) Retro Ignition
T I WE	(SEC)	150.3 151.0 151.3 152.3 152.8 (1) Retro
		(1)

MARSHALL SPACE FLIGHT CENTER

TABLE I-VII-H

S-I RETRO PORTION TRAJECTORY

					EARTH FI	FIXED PARAMETERS	TERS		j	LØNGITUDE	GEND. LAT.	GEOC. LAF.
	TIME	XXXE	YY YE	222E	DXXE	DYYE	DZZE	VELØCITY	PATH	(PØSILIVE WEST)	(PBSI IIVE NØRTH)	(PØSILIVE NØRTH)
	(SEC)	(X	(KM)	(KM)	(M/SEC)	(M/SEC)	(M/SEC)	(M/SEC)	(DEG)	(DEG)	(DEC)	(DEG)
(1)	150.3	82.6	89.8	7. 0	2168.6	1641.3	12.1	2719.7	52.13	79.7374	28.4616	28.3007
	151.0	84.0	6*06	7. 0	2165.0	1632.3	12.2	2711.4	52.23	79.7228	28.4603	28.2994
	151.3	84.7	91.4	7. 0	2162.8	1627.7	12.3	2706.9	52.27	79,7159	28.4597	28.2988
	152.3	86.9	93.0	4.0	2154.3	1612.1	12.4	2690.7	52.41	79.6945	28.4578	28.2968
(2)	152.8	87.9	93.7	4-0	2151.6	1605.9	12.4	2684.8	52.47	79.6850	28.4569	28.2960

(1) Retro Ignition (2) Retro E. T. D.

TABLE I-VII-I S-I COAST TO IMPACT TRAJECTORY

				7-770-7	משטד זה דתשה	Trengerous	,			
				MARSH/	ALL SPACE FL	FLIGHT	CENTER			
TIME	GRØUND DISTANCE	ALTI TUDE		SPACE FIXED PATH ANGLE	ACCELERATION V DOT	MASS	DYNAM IC PRESSURE	THRUST	MACH	DRAG
(SEC)	(KM)	(KA)	VELOCITY (M/SEC)	(DEG)	EARTH-FIXED (M/SEC SQ)	(KG)	(N/M SQ)	(N)		Ŝ
52.	6.5	4.3	023.	~	-5.80	311	z.	c	9	817
155.0	91.24	97.95	3011.8	57.54	-5.75	53117	m	0	9.32	419
61.	03.7	07.4	981.	æ	-5.62	311		0	3	8
67.	16.2	16.7	951.	0	-5.49	311	0	0	7	19
73.	28.7	25.6	923.	0	-5.36	311	0	0	8	
79.	41.1	34.2	895.	0	-5.22	311	0	0	6	
85.	53.5	45.6	868.	_	-5.08	311	0	0	3	
91.	5.9	9.0	841.	\sim	-4.94	311	0	0	6.	_
97.	78.5	58.3	816.	3	-4.80	311	0	0	٠,	-
93	90.5	65.7	791.	4	-4.65	311	0	0	'n	0
60	02.7	72.8	767.	S	-4.50	311	0	0	4.	0
15.	14.9	19.6	7 44.	9	-4.34	311	0	0		0
21.	27.1	86.2	722.	~	-4.19	311	0	0	.2	0
27.	39.3	92.4	701.	œ	4	311	0	0	. 1	0
9 60	51.4	98.3	580.	œ	-3.86	311	0	0	0	0
,	6.50	03.9	561.	9	-3.69	311	0	0	9	0
	75.6	09.2	543.	0	-3.52	311	0	0	6.	0
51:	87.6	14.2	525.	_	-3,34	311	0	0	٠,	0
67.	99.7	19.0	508.	2	-3.16	311	0	0	8	0
63.	111.7	23.4	593	4	N	311	0	0	8	0
69	23.7	27.5	578.	S	-2.79	311	0	0		0
75	35.7	31.4	564.	•	N	311	0	0		0
=	47.6	34.9	552.	_	-2.40	311	0	0	7.	0
. 6	59.6	38.2	540.	8	-2.21	311	0	0	•	0
93	71.5	41.1	530.	Ò	-2.01	311	0	0	9.	0
66	83.4	43.8	520.	0	-1.81	311	0	0	•	0
	95.4	46.1	511.	-	-1.60	311	0	Ó	•	0
• • • •	5.70	7*85	\$ 0.4°	2	~	311	0	0	• 5	0
• r c	7.61	0.0	s .	83.74	-1.18	311	0	0		0
	0.16	21.5	. 35	4	26.0-	311	0	0	เร	0
, ,	V . V .	52.7	• 88 •	5	-0.76	311	0	0	• 2	0
50	54.8	53.6	484.	-	-0.55	311	0	0	ť.	0
1	7.99	54.2	482.	œ	-0-33	311	0	0	Ţ,	0
*1.	78.6	544.5	481.	9	-0.12	311	0	0	\$	0
20.	85.3	54.5	¥81.	0	00.0	311	0	0	5	0
53.	90.4	54.5	481.	0	0.10	311	0	0	5	0
59.	02.3	54.2	482	91.62	0.31	311	0	0	ď	0
65	14.2	53.6	484.	2	0.53	311	0	0	'n	0
71.	26.1	521.8	487.	3.8	0.74	311	0	0	ď	0
77.	37.9	51.0	491.	4.9	0.95	311	0	0	ů	0

TABLE I-VII-I(CONT) S-I COAST TO IMPACT TRAJECTORY

MARSHALL SPACE FLIGHT CENTER

(KG) (N/M SQ 53117 0 53117 1673 0 53117 0 53117 0 53117 1673 0 53117 0 53117 1673 0 53117 23557 0	ALTITUDE	a.	SP	CELERATION	MASS	DYNAMIC	THRUST	MACH	DRAG
(KG) (N/M SQ) (N) 53117 0 2.57 53117 0 2.66 53117 0 2.67 53117 0 2.67 53117 0 2.67 53117 0 2.67 53117 0 2.78 53117 0 2.78 53117 0 2.85 53117 0 2.86 53117 0 2.85 53117 0 2.85 53117 0 3.29 53117 0 3.29 53117 0 3.26 53117 0 3.26 53117 0 3.26 53117 0 3.26 53117 0 4.91 53117 0 0 4.91 53117 0 0 2.64 53117 417 0 0 2.85 53117 417 0 0 0 2.94 53117 420 <td< th=""><th>FIXED PATH</th><th>PATH</th><th></th><th>V DØT EARTH-FIXED</th><th></th><th>PRESSURE</th><th></th><th></th><th></th></td<>	FIXED PATH	PATH		V DØT EARTH-FIXED		PRESSURE			
1.16 53117 0 2.57 1.58 53117 0 2.58 1.79 53117 0 2.64 2.19 53117 0 2.67 2.39 53117 0 2.67 2.96 53117 0 2.67 2.97 53117 0 2.67 3.32 53117 0 2.76 3.47 53117 0 2.78 3.50 53117 0 2.89 4.17 53117 0 2.89 4.23 53117 0 2.89 4.33 53117 0 2.89 4.48 53117 0 3.69 4.78 53117 0 3.69 4.78 53117 0 3.69 4.78 53117 0 3.69 4.78 53117 0 0 3.69 4.78 53117 0 0 3.69 4.78 53117 0 0 3.69 4.86 5311	È	_		(M/SEC SQ)	(KG)		(N)		Ŝ
1.37 53117 0 2.58 1.58 53117 0 2.64 1.99 53117 0 2.64 2.39 53117 0 2.67 2.39 53117 0 2.64 2.96 53117 0 2.67 3.14 53117 0 2.85 3.50 53117 0 2.86 3.50 53117 0 2.96 3.50 53117 0 2.96 4.17 53117 0 2.96 4.28 53117 0 2.96 4.33 53117 0 2.94 4.48 53117 0 2.94 4.78 53117 0 2.94 4.93 53117 0 0 3.29 4.78 53117 0 0 3.94 5.71 53117 0 0 2.94 5.71 53117 0 0 2.94 5.72 53117 0 0 3.94	0.20 2497.	6.1		7	311	0	0	Š	0
1.528 53117 0 0 2.64 2.19 53117 0 0 2.67 2.29 53117 0 0 2.67 2.29 53117 0 0 2.85 3.14 53117 0 0 2.85 3.20 53117 0 0 2.85 3.21 53117 0 0 2.85 3.22 53117 0 0 2.85 3.24 53117 0 0 3.06 4.48 53117 0 0 3.29 4.48 53117 0 0 3.29 4.29 53117 0 0 3.29 4.31 53117 0 0 0 3.29 4.32 53117 0 0 0 3.29 4.33 53117 0 0 0 3.29 4.34 53117 0 0 0 3.29 4.35 53117 0 0 0 3.29 4.36 53117 0 0 0 0 0.00 5.40 53117 1673 0 0 0 0.00 1.31 53117 48051 0 0 0.75 2.50 53117 5207 0 1.96 35 2.50 53117 5207 0 0 0.75 2.50 53 53117 5207 0 0 0.75 2.50 53 53117 5207 0 0.75 2.50 6.46 80 2.60 6.46 80 2.60 6.46 80 2.60 6.60 6	5 97.2	7.2		U,	311	0 (0 (ď.,	0 (
1.79 53117 0 0 2.64 2.39 53117 0 0 2.64 2.39 53117 0 0 2.69 2.47 53117 0 0 2.89 3.32 53117 0 0 2.89 3.34 53117 0 0 2.89 3.44 53117 0 0 2.89 4.48 53117 0 0 3.09 4.48 53117 0 0 3.69 4.49 53117 0 0 3.69 4.48 53117 0 0 3.69 4.49 53117 0 0 3.69 4.49 53117 0 0 3.69 4.49 53117 0 0 3.69 4.49 53117 0 0 3.69 4.51 53117 0 0 0 3.69 4.63 53117 0 0 0 3.69 4.64 53117 0 0 0 3.69 4.65 5.31 53117 0 0 0 3.69 4.67 53117 0 0 0 3.69 4.68 53117 1673 0 0 0.00 4.68 6.31 7 6.25 11.31 53117 6.25 11.39 53117 6.25 11.39 53117 5.40 11.30 53117 5.40 11.30 5.3117 5.40 11.31 5.3117 5.40 11.31 5.3117 5.40 11.39 5.3117 5.40 11.30 5.3117 5.40 11.31 5.3117 5.40 11.31 5.3117 5.40 11.31 5.3117 5.40 11.31 5.3117 5.40 11.31 5.3117 5.40 11.31 5.3117 5.40 11.31 5.3117 5.40 11.31 5.3117 5.40 11.31 5.3117 5.40 11.31 5.3117 5.40 11.31 5.3117 5.40 11.31 5.3117 5.40 11.31 5.3117 5.40 11.31 5.3117 5.40 11.31 5.3117 5.40 11.30 5.3117 5.40 11.30 5.3117 5.40 11.30 5.3117 5.40 11.30 5.3117 5.40 11.30 5.3117 5.40 11.30 5.3117 5.40 11.30 5.3117 5.40 11.30 5.3117 5.40 11.30 6.40 11.30	6.41 2510.9 98.3 6.41 2510.9	χ. 		Ů.	31.	> ()	۰٠	> (
2.19 53117 0 2.69 2.29 53117 0 2.73 2.96 53117 0 2.69 3.14 53117 0 2.89 3.26 53117 0 2.89 3.26 53117 0 2.89 3.44 53117 0 2.89 3.84 53117 0 2.89 4.01 53117 0 2.89 4.17 53117 0 3.06 4.18 53117 0 3.20 4.28 53117 0 3.29 4.29 53117 0 3.29 4.29 53117 0 3.29 4.34 53117 0 0 3.29 4.39 53117 0 0 3.29 4.49 53117 0 0 3.29 4.93 53117 2.20 0 0 5.21 53117 2.20 0 0 5.21 53117 2.35 0 0	4. US 25. 90.44	4.00		• 0	116	> c	-	۰	> C
2.39 53117 0 2.69 2.77 53117 0 2.78 2.39 53117 0 2.78 3.14 53117 0 2.85 3.29 2.31 0 2.94 3.50 53117 0 2.94 4.17 53117 0 2.94 4.21 53117 0 2.94 4.23 53117 0 2.94 4.33 53117 0 3.29 4.48 53117 0 3.29 4.93 53117 0 3.96 4.93 53117 0 3.96 4.93 53117 0 3.96 4.93 53117 0 3.96 4.93 53117 0 0 3.96 4.93 53117 0 0 3.96 4.93 53117 4.91 0 0 3.96 4.93 53117 4.17 0 0 0 3.96 4.94 53117 417 <td>1.001 5.250.2 101.3 8 53 5530.3 101.4</td> <td>300</td> <td></td> <td>•</td> <td>117</td> <td>o c</td> <td>> C</td> <td>•</td> <td>o c</td>	1.001 5.250.2 101.3 8 53 5530.3 101.4	300		•	117	o c	> C	•	o c
2.58 53117 0 2.75 2.96 53117 0 2.76 2.96 53117 0 2.85 3.14 53117 0 2.89 3.50 53117 0 2.86 3.67 53117 0 2.94 4.01 53117 0 3.06 4.17 53117 0 3.20 4.28 53117 0 3.29 4.29 53117 0 3.52 4.33 53117 0 3.52 4.29 53117 0 3.52 4.34 53117 0 3.52 4.93 53117 0 0 3.52 5.21 53117 0 0 3.52 5.21 53117 0 0 4.34 5.21 53117 0 0 0 9.66 5.21 53117 417 0 0 0 9.86 5.21 53117 417 0 0 0 0 9.8	5,31 2550.8 102	0.70		• (311	o c	0	9	oc
2.77 53117 0 2.76 2.96 53117 0 2.80 3.14 53117 0 2.89 3.32 53117 0 2.89 3.64 53117 0 2.89 3.84 53117 0 3.06 4.01 53117 0 3.29 4.17 53117 0 3.29 4.28 53117 0 3.29 4.63 53117 0 3.29 4.63 53117 0 3.69 5.07 53117 0 3.29 4.93 53117 0 3.69 5.21 53117 0 3.69 5.22 53117 0 4.34 5.31 0 0 3.69 5.21 53117 0 0 4.34 5.24 53117 14 0 0 9.16 5.27 53117 417 0	1.80 2563.4 103.7	03.7		3	311	0	0	_	0
2.96 53117 0 2.80 3.14 53117 0 2.85 3.32 53117 0 2.94 3.67 53117 0 3.00 3.67 53117 0 3.20 4.01 53117 0 3.20 4.17 53117 0 3.20 4.33 53117 0 3.20 4.48 53117 0 3.52 4.78 53117 0 3.52 4.93 53117 0 3.69 4.93 53117 0 3.69 4.93 53117 0 3.69 4.93 53117 0 3.69 5.21 53117 0 0 3.69 5.21 53117 2 0 4.91 5.24 53117 417 0 0 9.86 5.21 53117 417 0 0 9.29 6.24 53117 23082 0 0 9.29 120.37 53117<	7.99 2576.9 104	04.8		7	311	0	0	7.	0
3.14 53117 0 2.85 3.25 53117 0 2.89 3.67 53117 0 2.94 3.67 53117 0 3.06 4.17 53117 0 3.20 4.17 53117 0 3.29 4.48 53117 0 3.52 4.53 53117 0 3.54 5.21 53117 0 3.54 5.21 53117 0 3.54 5.21 53117 0 3.69 6.24 53117 0 0 3.69 6.27 53117 0 0 3.69 5.47 53117 2 0 0 9.86 5.71 53117 417 0 0 9.29 5.81 53117 417 0 9.29 6.84 53117 23.55 0 9.29 1.39 53117 23.62 0 9.29 165.37 53117 23.62 0 9.29	3.88 2591.5 105.8	05.8		6.	311	0	0	ω	0
3.32 53117 0 2.89 3.50 53117 0 2.94 3.67 53117 0 3.06 4.01 53117 0 3.20 4.33 53117 0 3.20 4.48 53117 0 3.29 4.78 53117 0 3.94 4.93 53117 0 3.94 5.07 53117 0 3.94 5.21 53117 0 3.94 5.24 53117 0 4.91 5.27 53117 0 0 3.94 5.21 53117 0 0 3.94 5.27 53117 0 0 9.26 5.81 53117 14 0 10.03 5.81 53117 417 0 9.26 6.81 53117 417 0 9.29 6.82 53117 5357 0 9.29 6.84 53117 5367 0 9.26 6.40 5311	9.48 2607.0 106.	.90		٦	311	0	0	8	0
3.50 53117 0 2.94 3.67 53117 0 3.06 4.01 53117 0 3.06 4.17 53117 0 3.20 4.48 53117 0 3.29 4.63 53117 0 3.29 4.63 53117 0 3.29 4.78 53117 0 3.29 4.93 53117 0 3.94 5.07 53117 0 3.94 5.21 53117 0 4.34 5.47 53117 0 0 4.91 5.21 53117 0 0 9.26 5.47 53117 14 0 10.03 5.71 53117 417 0 9.29 4.86 53117 417 0 9.29 5.13 53117 23.557 0 9.29 6.46 53117 23.62 0 9.29 6.45 53117 23.62 0 9.29 6.40 <	4.79 2623.4 107	07.		6	311	0	0	8	C
3.67 53117 0 3.00 4.01 53117 0 3.06 4.17 53117 0 3.20 4.33 53117 0 3.29 4.48 53117 0 3.52 4.78 53117 0 3.52 4.93 53117 0 3.94 5.07 53117 0 4.34 5.21 53117 0 4.34 5.24 53117 0 6.491 5.25 53117 0 6.491 5.21 53117 0 6.29 5.47 53117 2 0 8.26 5.71 53117 2 0 9.29 6.72 53117 417 0 9.29 6.12 6 6.46 86 5.31 6127 0 9.29 6.1.40 53117 23.557 0 8.21 6.1.40 53117 23.62 0 6.46 86 6.2.40 53117 52.62 0 0 9.29 6.2.40 53117 52.67 0 1.06 8.21 7.19 53117 52.67 0	9.79 2640.9 108.9	08.9		3	311	0	0	6	0
3.84 53117 0 3.06 4.01 53117 0 3.20 4.33 53117 0 3.29 4.48 53117 0 3.39 4.63 53117 0 3.69 4.93 53117 0 3.94 5.07 53117 0 4.34 5.21 53117 0 4.34 5.22 53117 0 4.34 5.21 53117 0 4.34 5.24 53117 0 4.34 5.27 53117 0 6.29 5.47 53117 2 0 9.26 5.12 53117 417 0 9.29 6.72 53117 417 0 9.29 4.86 53117 23557 0 9.29 4.86 53117 23627 0 9.29 4.86 53117 23082 0 9.29 4.86 53117 23082 0 9.29 4.86 53117	4.50 2659.2 109.9	6.60		•	311	0	0	0	0
4.01 53117 0 3.12 4.33 53117 0 3.29 4.48 53117 0 3.29 4.48 53117 0 3.94 4.93 53117 0 3.94 5.01 53117 0 4.34 5.07 53117 0 4.34 5.21 53117 0 6.26 5.47 53117 0 7.07 5.40 53117 0 0 9.16 5.71 53117 14 0 10.03 5.81 53117 417 0 8.75 2 6.71 53117 417 0 9.26 9.16 5.72 53117 417 0 8.71 36 6.71 53117 23.57 0 8.71 36 6.1.40 53117 23.557 0 8.71 36 6.40 53117 53.67 0 1.06 37.3 67 6.40 53117 5807 0	8.92 2678.5 110.	10.8		8	3	0	0	0	0
4.17 53117 0 3.20 4.38 53117 0 3.29 4.48 53117 0 3.39 4.78 53117 0 3.69 4.93 53117 0 3.94 5.07 53117 0 4.34 5.21 53117 0 4.34 5.34 53117 0 4.34 5.47 53117 0 0 4.34 5.41 53117 0 0 4.34 5.42 53117 0 0 9.16 5.71 53117 14 0 10.03 5.81 53117 417 0 9.29 4.86 53117 417 0 8.71 36 11.39 53117 23.557 0 6.46 86 120.37 53117 23.657 0 1.96 35 -59.53 53117 23.657 0 1.96 35 -59.53 53117 5807 0 0.75 6 <td>3.03 2698.8 111</td> <td>1</td> <td></td> <td>0</td> <td>m</td> <td>0</td> <td>0</td> <td>~</td> <td>0</td>	3.03 2698.8 111	1		0	m	0	0	~	0
4.33 53117 0 3.29 4.48 53117 0 3.39 4.93 53117 0 3.69 4.93 53117 0 3.94 5.07 53117 0 4.34 5.21 53117 0 4.34 5.34 53117 0 6.434 5.47 53117 0 0 4.34 5.41 53117 0 0 7.07 5.71 53117 2 0 9.16 5.71 53117 417 0 10.03 5.81 53117 417 0 9.29 4.86 53117 417 0 9.29 -61.40 53117 23.57 0 8.41 3 16.39 53117 23.557 0 6.46 8 120.37 53117 23.627 0 1.96 35 -59.53 53117 23.627 0 1.96 35 -59.53 53117 5807 0 0.75	6.84 2719.9 112	12			'n	0	0	.2	0
4.48 53117 0 3.39 4.63 53117 0 3.52 4.78 53117 0 3.94 5.07 53117 0 0 3.94 5.21 53117 0 0 4.34 5.24 53117 0 0 4.34 5.47 53117 0 0 7.07 5.41 53117 2 0 9.16 5.71 53117 14 0 10.03 5.81 53117 417 0 9.29 4.86 53117 417 0 9.29 -11.39 53117 417 0 8.21 36 -61.40 53117 23.557 0 8.21 36 120.37 53117 23.627 0 1.96 35 -59.53 53117 5807 0 1.09 18 -7.19 53117 5807 0 0.75 8	0.36 2741.9 113	13		ω,	n	0	0	.2	0
4.63 53117 0 3.52 4.78 53117 0 3.69 5.07 53117 0 0 4.34 5.21 53117 0 0 4.34 5.34 53117 0 0 4.91 5.47 53117 0 0 7.07 5.81 53117 2 0 9.16 5.81 53117 14 0 10.03 5.72 53117 417 0 9.29 4.86 53117 417 0 8.21 36 -11.39 53117 417 0 8.21 36 -11.39 53117 23.557 0 8.21 36 120.37 53117 23.627 0 1.96 35 -59.53 53117 5267 0 1.09 16 -7.19 53117 5267 0 0.75 6	3.58 2764.8 114	14		4.	n	0	0	3	0
4.78 53117 0 3.69 4.93 53117 0 3.94 5.07 53117 0 4.34 5.34 53117 0 6.491 5.47 53117 0 6.707 5.41 53117 0 7.07 5.81 53117 2 0 9.16 5.71 53117 14 0 10.03 5.72 53117 417 0 9.29 4.86 53117 417 0 9.29 -61.40 53117 23.57 0 8.21 36 -61.40 53117 23.57 0 8.21 36 120.37 53117 23.557 0 6.46 86 -59.53 53117 23.627 0 1.96 35 -59.53 53117 5267 0 0.75 8	6.49 2788.5 115	15		•	n	0	0	ŝ	0
4.93 53117 0 3.94 5.07 53117 0 6.34 5.34 53117 0 6.491 5.47 53117 0 7.07 5.60 53117 0 0 7.07 5.81 53117 2 0 9.16 5.71 53117 14 0 10.03 5.72 53117 417 0 9.29 4.86 53117 417 0 9.29 -11.39 53117 5357 0 8.41 9.29 -61.40 53117 23557 0 8.21 36 150.37 53117 23557 0 6.46 86 -59.53 53117 23082 0 1.96 35 -59.53 53117 5807 0 0.75 8 -7.19 53117 5267 0 0.75 6	9.11 2813.1 116	16		۲.	$\boldsymbol{\omega}$	0	0	•	1
5.07 53117 0 4.34 5.21 53117 0 6.91 5.47 53117 0 6.91 5.40 53117 0 0 7.07 5.41 53117 2 0 9.26 5.71 53117 417 0 9.29 5.72 53117 417 0 9.29 4.86 53117 417 0 9.29 -11.39 53117 23557 0 8.41 9.29 -61.40 53117 23557 0 8.21 36 -59.53 53117 23627 0 1.96 35 -59.53 53117 23082 0 1.96 35 -7.19 53117 5807 0 0.75 8 -7.19 53117 5267 0 0.75 6	1.42 2838.6 117	17		6.	m	0	0	••	~
5.21 53117 0 4.91 5.34 53117 0 0 5.78 5.47 53117 0 0 7.07 5.60 53117 14 0 10.03 5.72 53117 417 0 9.29 4.86 53117 417 0 9.29 1.31 53117 417 0 8.75 -11.39 53117 23.57 0 8.41 9 145.17 53117 23.57 0 8.41 9 150.37 53117 23.57 0 6.46 80 150.37 53117 23.62 0 6.46 80 -59.53 53117 23.62 0 1.96 35 -26.40 53117 5807 0 0.75 8 -7.19 53117 5267 0 0.75 6	3.43 2864.8 118	18		0	3	0	0	6	-
5.34 53117 0 5.78 5.47 53117 0 0 7.07 5.60 53117 2 0 9.16 5.81 53117 14 0 10.03 5.72 53117 417 0 9.26 4.86 53117 417 0 9.29 1.31 53117 417 0 8.75 2 -61.40 53117 23557 0 8.41 36 120.37 53117 52527 0 6.46 80 120.37 53117 23627 0 1.96 35 -59.53 53117 53627 0 1.96 35 -26.40 53117 5807 0 0.75 8 -7.19 53117 5267 0 0.75 6	5.14 2891.9 119	6		,7	m	0	0	4.91	2
5.47 53117 0 7.07 5.60 53117 0 8.26 5.71 53117 14 0 10.03 5.81 53117 417 0 9.26 4.86 53117 417 0 9.29 1.31 53117 417 0 8.75 -11.39 53117 6127 0 8.41 46.11 53117 23557 0 6.46 80 120.37 53117 52622 0 6.46 80 -59.53 53117 23682 0 1.96 35 -26.40 53117 5807 0 0.75 8 -7.19 53117 5267 0 0.66 6	6.55 2919.8 119	6		ć	m	0	0	5.78	s.
5.60 53117 0 8.26 5.71 53117 2 0 9.16 5.81 53117 14 0 10.03 4.86 53117 417 0 9.29 4.86 53117 417 0 8.75 -11.39 53117 6127 0 8.41 9 -61.40 53117 23557 0 8.41 9 120.37 5317 55422 0 6.46 80 -59.53 53117 23082 0 1.96 35 -26.40 53117 5807 0 0.75 8 -7.19 53117 5267 0 0.66 6	7.65 2948.4 120	20		4.	n	0	0	7.07	17
5.71 53117 2 0 9.16 5.81 53117 14 0 10.03 4.86 53117 417 0 9.29 1.31 53117 417 0 9.29 -11.39 53117 6127 0 8.41 5 -61.40 53117 23557 0 8.21 36 120.37 5317 55422 0 6.46 80 120.37 53117 23082 0 1.96 35 -59.53 53117 9827 0 1.09 18 -7.19 53117 5267 0 0.75 8	8.44 2977.9	21		٠	m	0	0	8.26	
5.81 53117 14 0 10.03 5.72 53117 417 0 9.29 4.86 53117 1673 0 9.29 11.39 53117 6127 0 8.41 9 -61.40 53117 23557 0 8.41 9 14.50.37 53117 55427 0 6.46 80 150.37 53117 23082 0 1.96 35 -59.53 53117 9827 0 1.96 35 -7.19 53117 5807 0 0.75 8	0.00 3004.7 122	22		•	n	~	0	9.16	262
5.72 53117 87 0 9.86 4.86 53117 417 0 9.29 1.31 53117 1673 0 8.75 2 -11.39 53117 6127 0 8.41 5 145.17 53117 23557 0 8.21 36 120.37 53117 48051 0 6.46 80 -59.53 53117 23082 0 1.96 35 -26.40 53117 5807 0 0.75 8 -2.88 53117 5267 0 0.66 6	9.11 3038.9 123	23		•	m	14	0	10.03	2246
4.86 53117 417 0 9.29 1.31 53117 1673 0 8.75 2 -61.40 53117 23557 0 8.41 9 145.17 53117 23557 0 6.46 8 120.37 53117 23622 0 6.46 8 -59.53 53117 23082 0 1.96 35 -26.40 53117 9827 0 1.09 18 -7.19 53117 5807 0 0.75 8 -2.88 53117 5267 0 0.66 6	8.99 3069.9 123	23		•	n	87	0	8	13643
1.31 53117 1673 0 8.75 2 -11.39 53117 6127 0 8.41 9 -61.40 53117 23557 0 8.21 36 145.17 53117 55427 0 6.46 8C 120.37 53117 48051 0 3.73 67 -59.53 53117 23082 0 1.96 35 -26.40 53117 9827 0 1.09 18 -7.19 5317 5267 0 0.75 8	8.56 3098.5 124	24		8	311	417	0	• 2	65571
-11.39 53117 6127 0 8.41 9 -61.40 53117 23557 0 8.21 36 145.17 53117 55422 0 6.46 8C 120.37 53117 48051 0 3.73 67 -59.53 53117 23082 0 1.96 35 -26.40 53117 9827 0 1.09 18 -7.19 53117 5267 0 0.75 8	7.86 3115.5 1.25	55		€,	311	1673	0	۲.	260288
-61.40 53117 23557 0 8.21 36 145.17 53117 55422 0 6.46 80 120.37 53117 48051 0 3.73 67 -59.53 53117 23082 0 1.96 35 -26.40 53117 9827 0 1.09 18 -7.19 53117 5807 0 0.75 8 -2.88 53117 5267 0 0.66 6	6.98 3090.0 12	25.9		11.3	31	6127	0	4.	941291
145.17 53117 55427 0 6.46 80 120.37 53117 48051 0 3.73 67 -59.53 53117 23082 0 1.96 35 -26.40 53117 9827 0 1.09 18 -7.19 53117 5807 0 0.75 8 -2.88 53117 5267 0 0.66 6	6.27 2898.8 126.3	6.3		61.4	31	355	0	.21	3604040
120.37 53117 48051 0 3.73 675426 -59.53 53117 23082 0 1.96 354142 -26.40 53117 9827 0 1.09 181264 -7.19 53117 5807 0 0.75 82887 -2.88 53117 5267 0 0.66 62954	6.99 2258.7 125.	25.6		145.1	31	542	0	.46	8060514
59.53 53117 23082 0 1.96 354142 26.40 53117 9827 0 1.09 181264 -7.19 53117 5807 0 0.75 82887 -2.88 53117 5267 0 0.66 62954	0.81 1411.0 122.5	22.5		120.3	311	805	0	.73	6
26.40 53117 9827 0 1.09 181264 -7.19 53117 5807 0 0.75 82887 -2.88 53117 5267 0 0.66 62954	7.41 890.9 117.4	17.4		59.5	311	308	C	96	
-7.19 53117 5807 0 0.75 82887 -2.88 53117 5267 0 0.66 62954	5.51 650.6 112.3	12.3		26.4	311	982		50	1 4
2.88 53117 5267 0 0.66 62954	4.24 555.2 109.	9.7		7.1	311	BO		7.5	
•682 93116 0 0.66 62954	2000 7000 7000 7000	• 0		• 6	7 7 7	3	> 0	•	1007
	3.16 519.1	•		•	3	76	Э	٥	2954

				MARSHA	TABLE I-VII-I (CONT) S-I COAST TO IMPACT MARSHALL SPACE FLIGHT	LIGHT	CENTER			
TIME	GRØUND DISTANCE	ALTITUDE	SPACE FIXED VEL ØCITY	SPACE FIXED Path angle	ACCELERATION V DOT EARTH-FIXED	MASS	DYNAM IC Pressure	THRUST	MACH	DRAG
(SECI)	(KK)	(KM)	(N/SEC)	(DEC)	(M/SEC SQ)	(KG)	(N/M SQ)	œ E		ŝ
623.0	976.63	12.12	495.5	110.12	-1.84	53117	5206	0	09.0	593282
629.0	949.98	11:11	478.2	110.09	-1.56	53117	5241	0	0.56	589202
635.0	911.06	10.15	465.1	109.79	-1.38	53117	5266	0	0.52	585361
0.149	977-17	9.22	455.3	109.31	-1.24	53117	5280	0	0.49	581012
0.749	977.25	8.34	448.0	108.73	-1.12	53117	5281	0	0.46	576051
653.0	977.30	7.49	442.7	108.12	-1.01	53117	5278	0	0.43	571101
659.0	977.33	6.68	438.7	107.51	-0.92	53117	5273	0	0.41	566517
665.0	977.35	5.91	435.7	10,901	-0.86	53117	5267	0	0.39	563157
671.0	977.36	5.16	433.3	106.32	-0.80	53117	5254	0	0.37	560090
677.0	977.37	4.45	431.5	105.76	-0.74	53117	5238	0	0.35	556963
683.0	75.776	3.76	458.9	105.23	-0.68	53117	5223	0	0.34	553997
0.689	977.38	3.09	428.7	104.73	-0.63	53117	5209	0	0.32	551258
695.0	977.38	2.45	457.6	104.26	-0.58	53117	5195	0	0.31	548701
701.0	977.38	1.83	426.7	103.83	-0.54	53117	5182	0	0.30	546282
707.0	977.38	1.22	425.9	103.43	64.0-	53117	5169	0	0.29	543965
713.0	977.38	0.64	425.1	103.06	-0.45	53117	5155	0	0.28	541716
719.0	977-39	0.07	424.5	102.73	-0.41	53117	5142	0	0.27	539516
719.8	977.39	00.0-	454.4	102.68	04.0-	53117	5140	0	0.27	539239

(1) Theoretical Ballistic Impact

28

TABLE I-VII-J S-I COAST TO IMPACT TRAJECTORY MARSHALL SPACE FLIGHT CENTER

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				EARTH FIX	XEC PARAMETERS	TERS		PATH	LØNGITUDE (PØSITIVE	GEBD. LAT.	GEBC. LAT.
TIME	XXXE	YYYE	222E	DXXE (M/SFC)	CYYE (M/SFC)	DZZE (M/SEC)	VELØCITY (M/SEC)	ANGLE (DEG)	WEST)	NØRTH)	NØRTH)
ב ב									! !) 	
52.			4.0	151	65.	2.	684.	52.47	9.685	.456	8.296
55.	2		4.0	2150.8	1585.3	•	2671.9	52.17	79.6375	28.4526	•29
61.	05.	90	0.5	148	30.	ä		3.6	9.510	.440	8.280
67.	18.	15.	9.0	146	75.			4-4	9.38	•459	٠. ش
73.	31.	24.	0.7	144	420-	5		5.3	9.256	.417	8,256
79.	44.	32.	0.8	142	65.	•	_	6.2	9.130	.405	8:244
85.	57.	40,	6.0	139	10.		2509.3	7	9.00	• 39	8.232
91.	.69	48.	1.0	137.	256.	œ		8.0	8.87	• 38	8.219
97.	82.	55.	1.1	134	CJ	9	-	0	78.7548	.3	8,207
03.	95.	62.	1.2	132	47	•		6.6	.63	• 35	8.194
.60	08.	.69	1.4	129	93	-		0	. 50	• 34	8.182
15.	21.	76.	1.5	127	39	2.		62.01	.382	• 32	8.169
21.	33.	82.	1.6	124	85	ω,	-	63.05		• 3	8.156
27.	46.	87.	1.8	121	32	4.		64.12	136	• 30	8.143
33.	59.	93.	1.9	118	78	\$	2293.9	65.21	013	• 29	8.129
39.	71.	98.	2.1	116	24	•	-	•	.891	.27	9.116
5.	84.	03.	2.3	113	71	Ļ	-	4.	. 768	٠,	8.102
51.	97.	07.	2.4	110	718.1	8		8.6		2	8.089
57.	10.	115	2.6	2106.9	664.8	•	2209.5	7.	77.5253		8.0
63.	22.	15.	2.8	103	611.7	ċ		0		?	8.061
69.	35.	19.	3•0	100.	58	,		72.18		-5	8.047
75.	47.	22.	3.1	160	0.5	÷		\sim		∹	8.033
81.	60.	25.	3,3	.460	52	2.		4		∹	8.018
87.	72.	27.	3.5	20602	66	3.		S		٦.	8.004
93.	85.	29.	3.7	087	46	4.	_	7.2		۳.	7.989
•66	98.	31.	4.0	083	63	5	-	8.5	.67	~	7.974
05.	10.	33.	4.2	2080-3	41	•	•	9	Z.	~	7.959
11.	22.	34.	4.4	910	88	÷	_	1.1	43	٦.	1.944
17.	35.	35.	4.6	073	35	æ		2	32	0	7.929
23.	47.	36.	4. 8	690	83.1	œ	•	3.8	6.20	•	7.913
29.	60.	36.	5.1	065	30.4	6	2066.1	Š	• 08	• 05	98
35.	72.	36.	5.3	061	-22.2	•	-	•	2.96	40.	7.882
41.	85.	36.	5.6	057	74	•	2059.6	87.87	. 84	28.0261	27.8668
47.	97.	35.	5.8	053	127	5	_	6	5.72	٥.	7.850
50.	04.	35.	0.9	051	157	•		ċ	5.65	00•	.841
53.	.60	34.	6.1	049	179	2.	2058.1	ċ	99.	• 99	4
59.	21.	33.	6.3	045	232	•	_	1.9	5.48	116.	.818
65.	34.	32.	9.9	041	85		2061.9	•		6.	8
71.	46.	30.	6.9	037.	337			4.6	5.24	944	7.785
377.0	558.6	228.1	7.1	2033.1	-380.3	9		6.0	5.12	927	. 768
		! !									

TRAJECTORY	CENTER
S-I COAST TO IMPACT	D.H.
5 13	$\stackrel{\smile}{=}$
COAST	II II
S-I	SPACE
(CONIT)	_
I-VII-J	SHAI
TABLE :	MAR

						!					
				EARTH F	FIXED PARAMETERS	TERS		DATH	LØNGITUDE	GEND. LAT.	GEØC. LAT.
TIME (SEC)	XXXE (KM)	YY YE	222E (KM)	DXXE (M/SEC)	DYYE (M/SEC)	DZZE (M/SEC)	VELØCITY (M/SEC)	ANGLE (DEG)	WEST) (DEG)	NØRTH)	NØRTH) (DEG)
383.0	570.8	25.	•	028.	442.	6.8		7.3	٠,	910	
6	•	22.		024.	495.	7.6	÷	8.6	ω,	.893	
ŝ		219.6	•	020	8	8.3	å	•	-		
-		16.		015.	.009	9.1	ë	1.3	•	.858	
÷	•	12.	•	010.	ë.	9.8	Š	2.6	r.	.840	
ë		90		900	•	0.5		3.8	4	.822	
ô	•	04.		001.	-759.2	1.3	-:	105.16	7	804	
ŝ	•	*66		966	812.	2.0	÷	9	Ξ.	. 786	
ä		94.	6	991.	864.	2.7	å	7	9	.768	
7		88.	ċ	986		3.4	ċ	108.80	5	.749	
8	•	83.	ċ	981.	970.	4.0		0	ω.	27,7310	
6	•	77.	ċ	976.		4.7	7	111.23	φ.	27.7121	
Š		6.	÷	971.	077.	5.4	2	\$	ະເຄ	27.6930	
-	•	64	ï	996	130.	0.9	ċ	13.	4	27.6738	
-	•	57:	÷	961.	183.	6.7	_:	•	L.	27.6543	
'n	•	50.	5	955.	237.	7.3	ŝ	15.	~	27.6347	
ď	•	45.	5	950.	290.	8.0	å	116.79	٠.	27.6149	
ŝ	•	34.	2	945.	344.	9.6	÷	17.	5	27.5948	
-	•	26.	ë.	939.	-1398.1	9.2	÷	18.	Φ,	27.5746	
.	•	17.	3	933.	452.	8.6	÷	19.	-	27.5542	
ė	•	08.	ů,	928.	505	4.0		20.	ď	27.5335	
ď,			†	922.		6.0	÷	-	4	27.5127	
5	•	•	4	916.	614.	1.5	÷	22.	ď	27.4916	
;		•	Š	910.	æ	2.1	÷	23.	~	27.4704	
٠,	•		ń	904.	722.	2.6	÷	÷	٦.	27.4489	
3	•		Š	898.	777.	3.2	_:	25.	6	27.4272	
539.0	877.2	48.9	16.1	1891.8	-1832.3	63.7	2634.4	126.27	71.8600	27.4053	27.2483
٠,			ġ.	886.	1881.	4.1		27.	_	27.3856	
:			•	878	1942.	÷	2703.1	•	ō	27.3607	
		•	-	871.	966			28.	4	27.3381	
ě		•	-	862.	049.	Š	់	29.	ď.	27,3153	
ė.	•	10,	æ	845.	2093.	Š	÷	ċ	~	27.2923	
Š		22.	æ	199.	103.	;	Ġ.	30.	7	27.2693	
	•	•	æ	646.	986	6	ំ	Ϊ,	٠,	27.2471	
-		45.	6	211.	ġ	;	÷	2.	9.8	, 228	
ě	•		è.	55.	869.	;	å	4.	9.0	,216	
ď		56.	6	12.	463.	11.8	÷	137.21	70.7921	27.2100	
5	•	6	6	49.	9	•	:	5	0.776	, 206	
:		9	6	6	•	•	-	•	0.767	205	
		61.	9.	•	86.	•	-	.	• 762	204	•

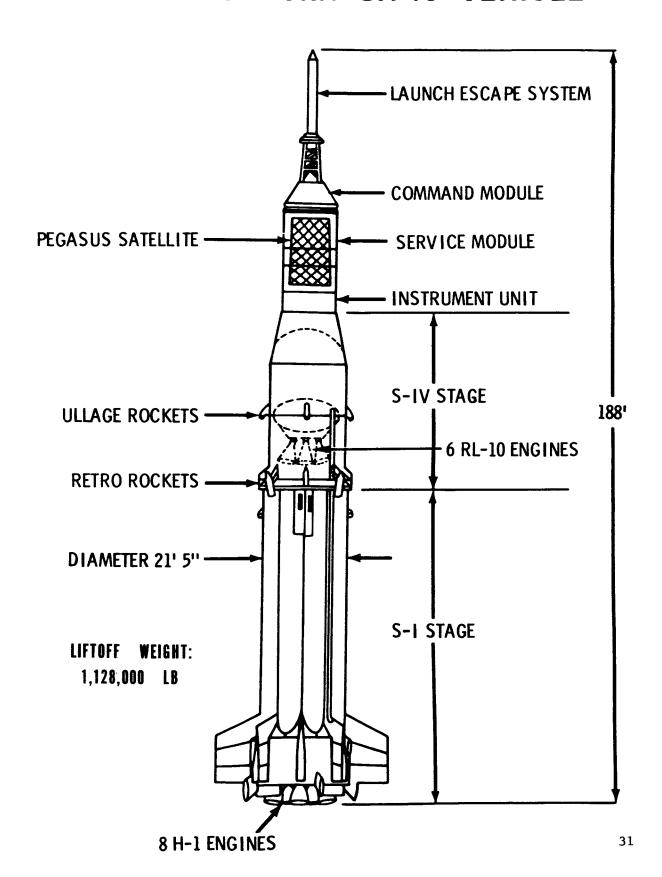
			TABLE I-VI	TABLE 1-VII-J(CONT) S-I COAST TO IMPACT THE MARSHALL SPACE FLIGHT C	S-I COAST IN	O IMPACT TRA-	TRAJECTORY			
			EARTH F	IXED PARAME	TERS			LØNGITUDE	GEBD. LAT.	GEØC. LAT.
XXXE (KM)	YYYE (KM)	222E (KM)	DXXE (M/SEC)	DYYE (M/SEC)	DZZE (M/SEC)	VELØCITY (M/SEC)	ANGLE (DEG)	MEST) (DEG)	NØRTH) (DEG)	NØRTH)
974.5	-62.6	19.6	24.9	-176.4	1.3	178.1	163.16	70.7585	27.2036	27.0474
974.6	-63.6	19.6	9.6	-167.7	7.0	168.0	16.791	70.7559	27.2031	27.0469
9.416	9.49-	19.6	8-0-	-159.2	0.3	159.2	171.48	70.7542	27.2027	27.0466
974.6	-65.5	19.6	T.T-	-151.1	0.0	151.3	174.11	70,7531	27.2025	27.0464
974.5	-66 4	19.6	-12.1	-143.7	-0-1	144.2	175.99	70,7523	27.2023	27.0462
974.4	-67.3	19.6	-14.7	-137.0	-0.2	137.8	177.30	70,7519	27.2022	27.0461
974.3	-68.1	19.6	-16.1	-131.0	-0-3	132.0	178.20	70,7516	27.2022	27.0460
974.2	-68.8	19.6	-16.8	-125.6	4.0 -	126.7	178.81	70.7514	27.2021	27.0460
974.1	9.69-	19.6	-17.0	-120.6	4.0-	121.8	179.20	70.7512	27.2021	27.0459
974.0	-70.3	19.6	-16.9	-115.9	-0-4	117.2	179.46	70,7512	27.2020	27.0459
973.9	-71.0	19.6	-16.6	-1111.7	4.0-	112.9	179.61	70.7511	27.2020	27.0459
973.8	-71.6	19.6	-16.2	-107.8	7. 0-	109.0	179.71	70.7511	27.2020	27.0459
973.7	-72.3	19.6	-15.8	-104.2	+0 <u>-</u> 0	105.4	179.76	70.7511	27.2020	27.0458
973.6	-72.9	19.6	-15.3	-100.8	-0-3	102.0	179.79	70.7510	27.2020	27.0458
973.6	-73.5	19.6	-14.9	-67.8	-0-3	6*86	179.81	70,7510	27.2019	27.0458
973.5	-74.1	19.6	-14.5	-95.0	-0-3	96.1	179.82	70.7510	27.2019	27.0458
973.4	-74.6	19.6	-14.1	-92.4	-0.3	93.5	179.82	70.7510	27.2019	27.0458
973.4	-74°7	19.6	-14.1	-55.1	-0-3	93.2	179.82	70.7510	27.2019	27.0458

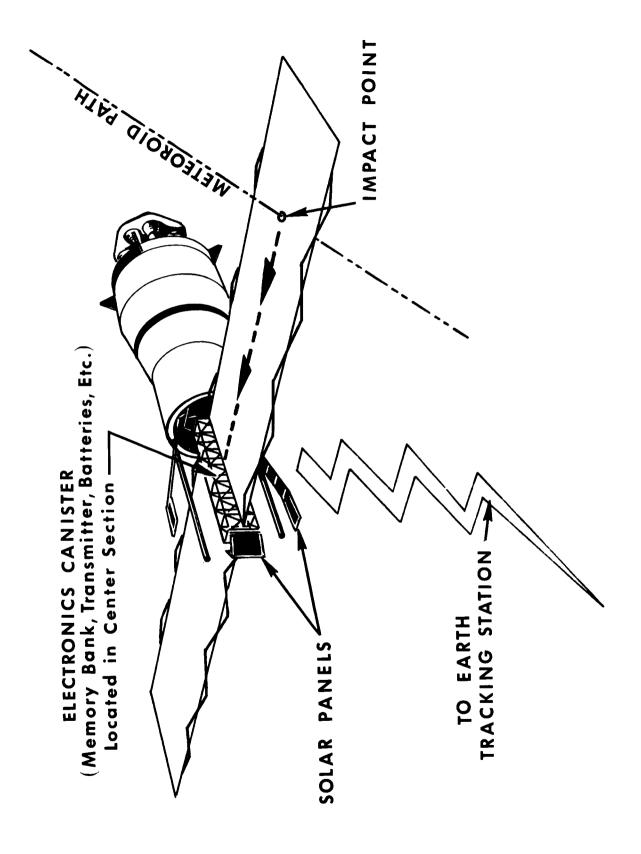
(1) Theoretical Ballistic Impact.

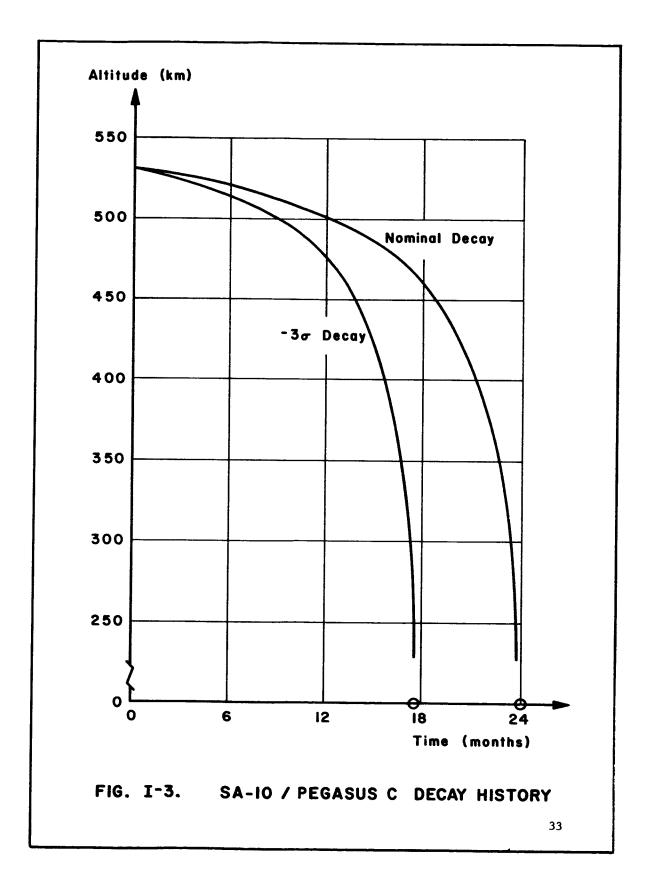
623.0 629.0 635.0 641.0 647.0 653.0 653.0 677.0 683.0 683.0 683.0 683.0 701.0

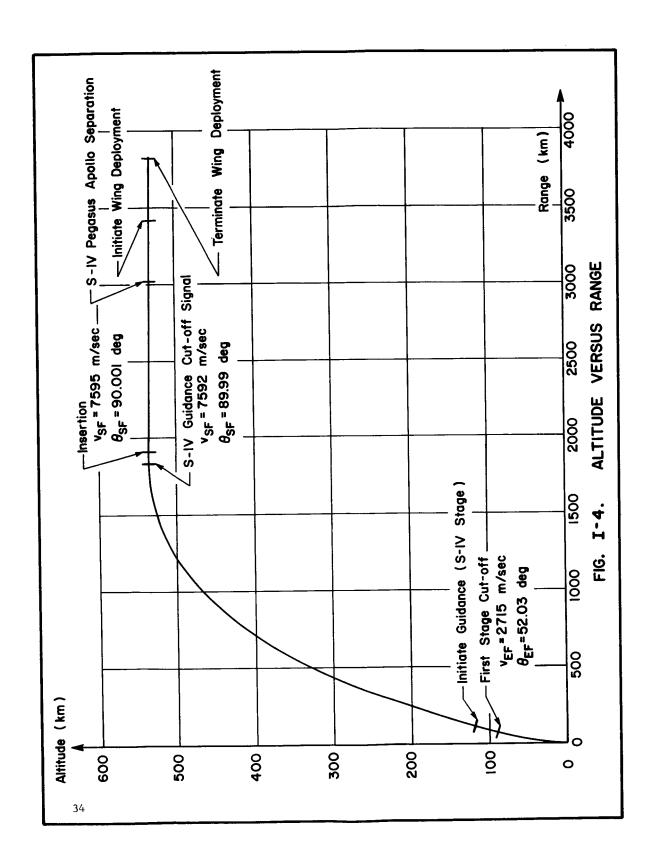
TIME (SEC)

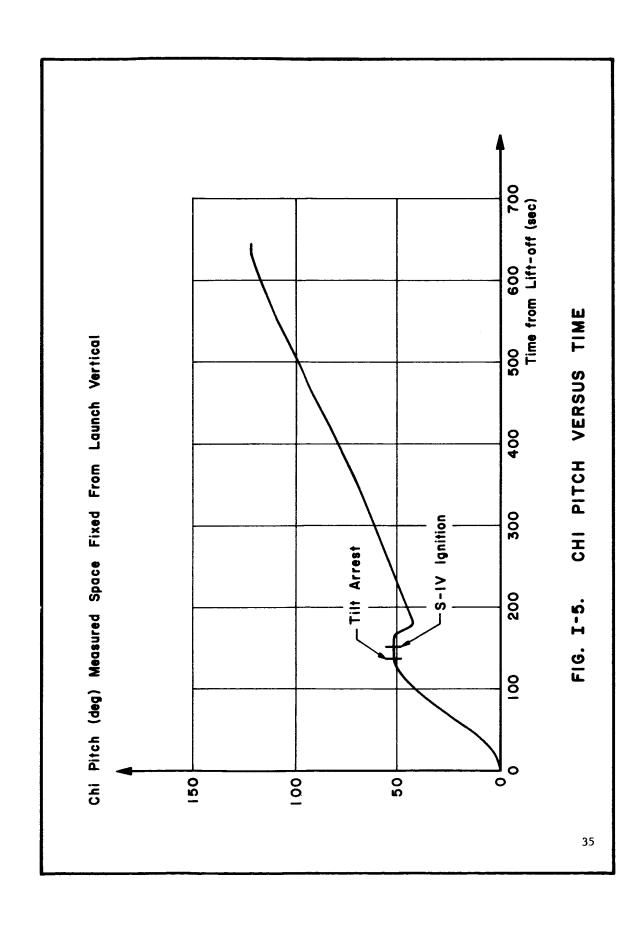
FIG. I-1. SATURN SA-10 VEHICLE











PART II

LAUNCH CRITERIA AND ORBITAL VENTING STATUS

A. LAUNCH CRITERIA

TO

Distribution

Mr. Sullivan/pac/876-3579 DATE June 24, 1965 R-AERO-FM-21-65

FROM

Chief, Flight Mechanics Branch, R-AERO-FM

SUBJECT Wind Launch Criteria for SA-10

REFERENCE

- (a) R-P&VE-SLL-65-6, "Structural Strength of SA-8 and SA-9 Vehicles," January 22, 1965
- (b) SA-10 Preliminary Predicted Trajectory, Unpublished
- (c) Saturn I, Block II Design Criteria Book
- (d) M-AERO-G-53-63, "Cape Canaveral, Florida, Wind Profile Envelopes for Selected Flight Azimuths," March 28, 1963
- (e) I-MICH-OA Letter Dated June 3, 1965
- 1. Wind speed limits for the SA-10 vehicle have been determined for the maximum dynamic pressure time point (t = 68 sec). These limits are established based on structural capabilities of the space vehicle as given in Reference (a). The structural capabilities of the space vehicle have been coordinated with MSC and are in agreement with structural limits imposed by them. Structural data furnished are a function of angle of attack (α), gimbal angle (β), and dynamic pressure (q). Disturbances other than the wind used to establish these limits are 99% shears and gusts (Reference (c), 3 α c₁ and c variations, and \pm 10% variation in the control gains. Trajectory data used are those obtained from Reference (b).
- 2. Figure 1 shows the wind speed limits as a function of wind azimuth for the maximum dynamic pressure time point (t = 68 sec). This figure shows the limits for various assumptions and combinations of disturbances upon which a decision for launch might be based. Wind magnitudes within the shaded portion of the figure could cause launch problems and a preflight simulation would be necessary for a launch decision. Wind magnitudes above the shaded portion of the figure could cause launch problems or make launch impossible. Wind magnitudes below the shaded portion create no apparent launch problems. But, under exceptional conditions, even winds of this magnitude may still lead to structural problems; therefore, a limited amount of flight simulation will still be performed.
- 3. Figure 2 shows the limiting wind from the most critical direction probability-wise, which is the tailwind. These wind limits are shown over flight time, assuming the same disturbances and combination of disturbances as used for Figure 1. Also shown on this figure is the 3 σ wind for the month of July (Reference (d)). Figure 3 shows the angle-of-attack limit and gimbal angle limit as a function of flight time for the same disturbances.

The gimbal angle limit shown here is derived in combination with the angle-of-attack limit and does not utilize the full gimbal angle capability of the vehicle, which is eight degrees. Also shown on this figure are the angle-of-attack and gimbal angle for the $3\,^{\circ}$ July wind as a function of flight time. Predicted median winds for July are less than $5\,$ m/s and, therefore, are not shown since their effect would be negligible.

4. The Saturn Block II vehicle, fueled, was designed to be structurally capable of withstanding the highest wind speed that may occur 99.9 per cent of the time, during any monthly period, while free-standing on the launch pad. During periods when ground wind conditions are predicted to exceed the 99.9 per cent peak wind speeds, the vehicle must be placed in a service structure or secured in such a manner that no additional wind loading conditions will be encountered by the vehicle; otherwise a risk of loss due to structural failure must be assumed. The free-standing SA-10 vehicle, unfueled, can withstand peak winds of approximately 34.7 knots (Reference (e).

Surface Wind Restriction: Referenced to 60 feet above natural grade.

	Steady State Velocity (knots) (m/sec)		Peak Velocity (knots) (m/sec)		
Vehicle Free-Standing (Fueled)	33 max	16.9	46 max	23.7	
Launch Release	20 max	10.3	28 max	14.4	

Using the 60 foot reference level (as agreed on between KSC and MSFC) the vehicle cannot be launched during peak winds exceeding 14.4 m/sec at this level. The probability of a peak wind exceeding 14.4 m/sec at 60 foot level above natural grade during July (excluding hurricanes) is less than .005. Winds of this magnitude create no control or collision problems during liftoff. If the launch should be made in August, the restrictions are less severe since the predicted winds for August are lower than predicted winds for July.

L. O. Stone

APPROVAL:

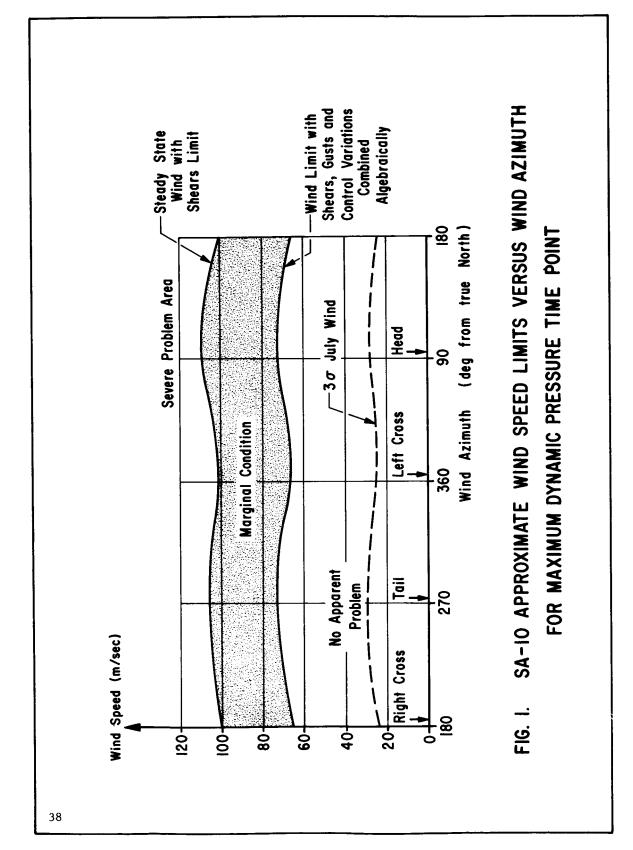
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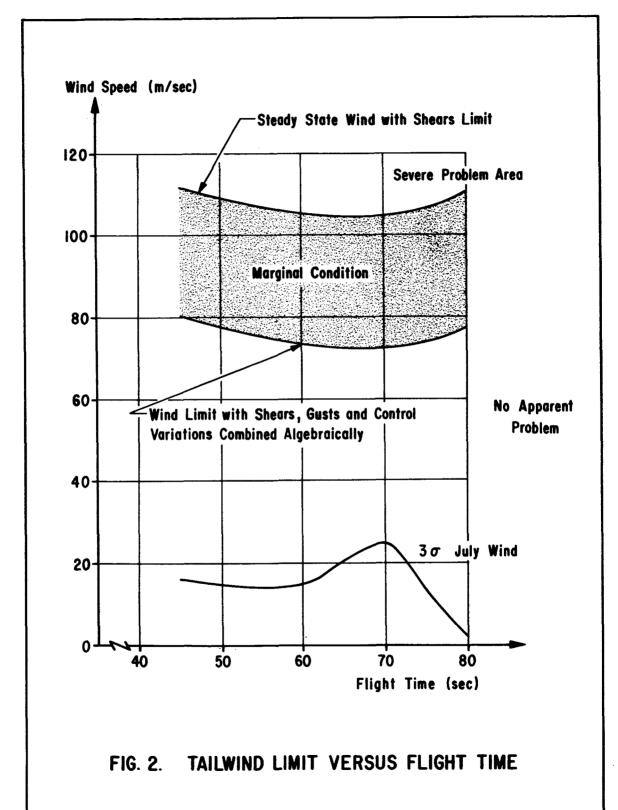
C.A. Kroll, R-P&VE-S

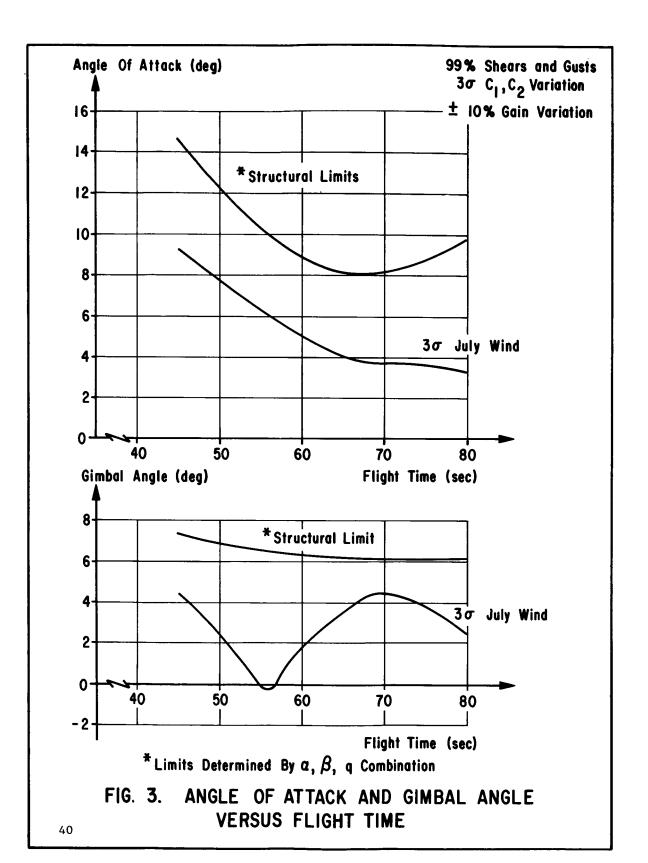
E. D. Geissler, R-AERO-DIR

H. H. Hosenthien, R-ASTR-F

3 Enc: Figures 1-3







B. ORBITAL VENTING STATUS

The SA-10 post insertion venting analysis provides a 95.5% confidence level of not exceeding the 9 deg/sec roll and 2 deg/sec tumble rate limits outlined in Reference 6. This analysis reflects the structural changes that are being incorporated for this vehicle; i.e., the interchange of 0_2 and H_2 non-propulsive vents. It also includes the best estimate of impingement effects of vented H_2 gases on the Pegasus wing structure (based on SA-9 flight evaluation data), as well as perturbations due to misalignments, c.g. shifts, etc.

PART III

Range Safety Data Summary for SA-10

The range safety data presented in Reference 7 consists of booster and LES impact areas, effects of range safety flight termination, land impact probabilities, injury probabilities, turning rate effects and other pertinent information.

The following parameters were varied to obtain the 3 ° envelope for range safety purposes: thrust, flow rate, liftoff weight, and wind speed. Impact data for this envelope is given in tabular form and consists of instantaneous cutoff time, geodetic latitude, longitude, remaining flight time, and range along the earth's surface from launch to impact. (See Reference 7).

The vehicle velocity vector turning data for the nominal trajectory is graphically presented. In particular, the total velocity vector magnitude and orientation in the lateral direction is presented as a time function from the point of malfunction (engine gimbal deflection), applied in the yaw plane. (See Reference 7).

The probability of the S-IV stage dropping short of orbital insertion is .13. The probability of impacting on land can be calculated as follows:

$$P_{\text{I}} = \frac{\triangle t}{T_{\text{B}}} \qquad \text{X} \qquad P_{\text{F}}$$

 $P_{\rm I}$ = probability of impacting on land area

 \triangle_{t} = dwell time (IIP transit time)

 T_B = total burn time of second stage

 P_{F} = probability of any failure causing the 2nd stage to drop short.

For SA-10:
$$P_{I} = \frac{4.9}{480.1}$$
 X .13 = 1.3 X 10⁻³

PART III (CONT'D)

Subdividing the impact probabilities for individual countries:

Land Area	Dwell Time	Impact Probability
Angola	2.8	7.6 X 10-4
Rhodesia & Nyasaland	1.5	4.1 x 10-4
Bechuanaland	.1	2.6 x 10-5
Mozambique	.3	8.1 x 10 ⁻⁵
Madagascar	.2	5.3 x 10-5

The probability of injuring a person downrange can be determined in the following manner:

$$P_{IP} = P_{I} \times \frac{N}{L_{A}} \times A_{L}$$

where

 P_{IP} = probability of injuring a person

 $\frac{N}{L_A}$ = population density of country

 A_L = lethal area

The probability of injuring a person, by overflying land is:

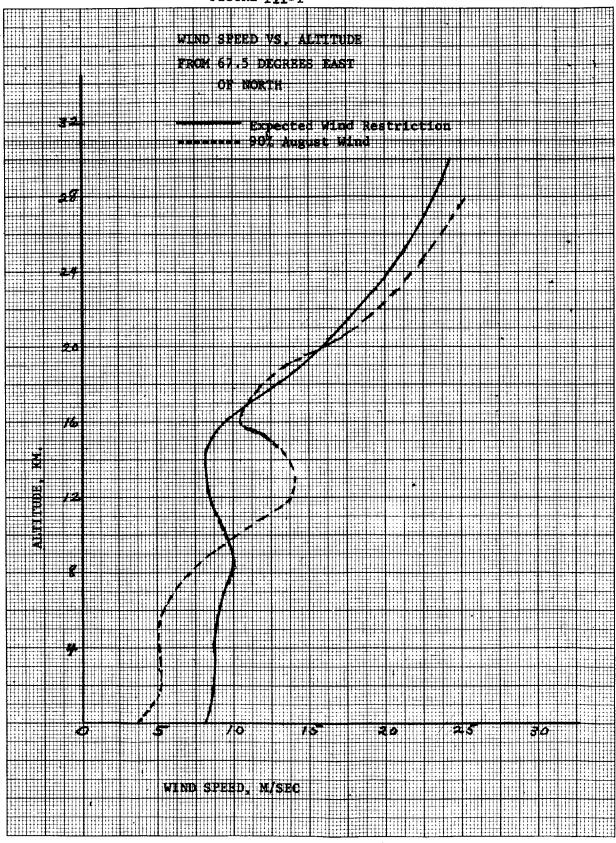
$$P_{TP} = 4.7 \times 10^{-6}$$

The probability of injuring a person, subdivided by Nation:

	N/ LA						
Nation	${ t P}_{ t I}$	(Per Sq. Mi.)	$\mathtt{P}_{\mathbf{IP}}$				
Angola	7.6 X 10-4	25	3.4 X 10-6				
Rhodesia & Nyasaland	4.1 X 10 ⁻⁴	12	8.8 x 10-7				
Bechuanaland	2.6 X 10-5	1	4.7 x 10-9				
Mozambique	8.1 x 10 ⁻⁵	25	3.6 x 10-7				
Madagascar	5.3 X 10 ⁻⁵	21	2.0 x 10-7				

PAD AREA STUDY

To avoid any impact of maximum distance pieces due to destruct, on critical areas, the wind profile in Figure III-1 should not be exceeded.



PART IV TRACKING

Data pertinent to the expected ground coverage of the SA-10 vehicle for primary tracking and telemetry stations are presented. Tracking coverage during the powered flight phase will be provided by C-band radar, ODOP Uprange, GLOTRAC, MISTRAM and close-in optical systems. For orbital flight C-band radars will provide coverage for about five revolutions after which MINITRACK will be the sole tracking source.

Powered Flight

A map defining the vehicle ground trace during powered flight and the coverage redundancy for primary ground sites is shown in Figure IV-1. As seen in the map, the entire powered flight is visible through the period of the Pegasus wing deployment to at least one ground station with a minimum of three station coverage to the time of shroud separation.

A detailed assessment of the visibility of the vehicle to each ground station scheduled to receive telemetry data and track the onboard electronic systems is presented in Figures IV-2 through IV-9. Elevation angle and slant range histories are shown from liftoff through Pegasus wing deployment or loss by the last C-band radar at Antigua. The Antigua station views the final deployment phase at a minimum elevation angle of 7 deg and a maximum slant range of 2000 km.

Elevation and slant range histories for the Green Mountain station at Huntsville, Alabama, are given in Figure IV-10. The maximum elevation angle reached for Green Mountain is 9.5 deg with an elevation of approximately 1 deg at S-IV cutoff.

The Fort Myers MINITRACK station will also provide coverage during powered flight. Slant range, elevation angle and azimuth angle histories are given in Figure IV-11. Fort Myers views S-IV cutoff at an elevation of 5 deg, an azimuth of 89 deg East-of-North and a slant range of 2110 km.

Orbital Flight

Primary tracking immediately following S-IV cutoff and insertion into orbit is provided by C-band radar stations. A summary of this coverage is given in Table IV-I.

TABLE IV-I Post Insertion Ground Coverage

Station	Elevation at S-IV Cutoff	Time Above Zero Deg Elevation
MILA	7 d e g	105 sec
Patrick	7	105
Grand Bahama	11	150
Grand Turk	23	245
Bermuda	29	310
Antigua	25	410

The locus of ground projections during the initial five orbital revolutions, with the ground network and visibility areas for C-band radar and MINITRACK superimposed, are shown in Figures IV-12 and IV-13, respectively.

Close approach range and maximum elevation angles for each of the first five revolutions are tabulated in Table IV-II for those stations having maximum elevation angles of at least 10 deg.

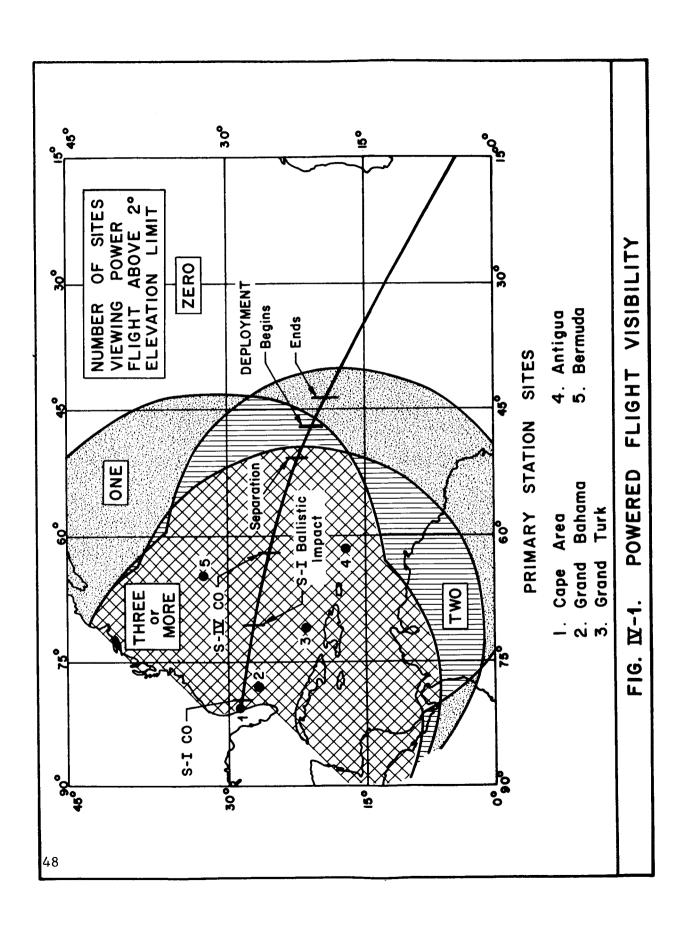
TABLE IV-II Orbital Ground Coverage

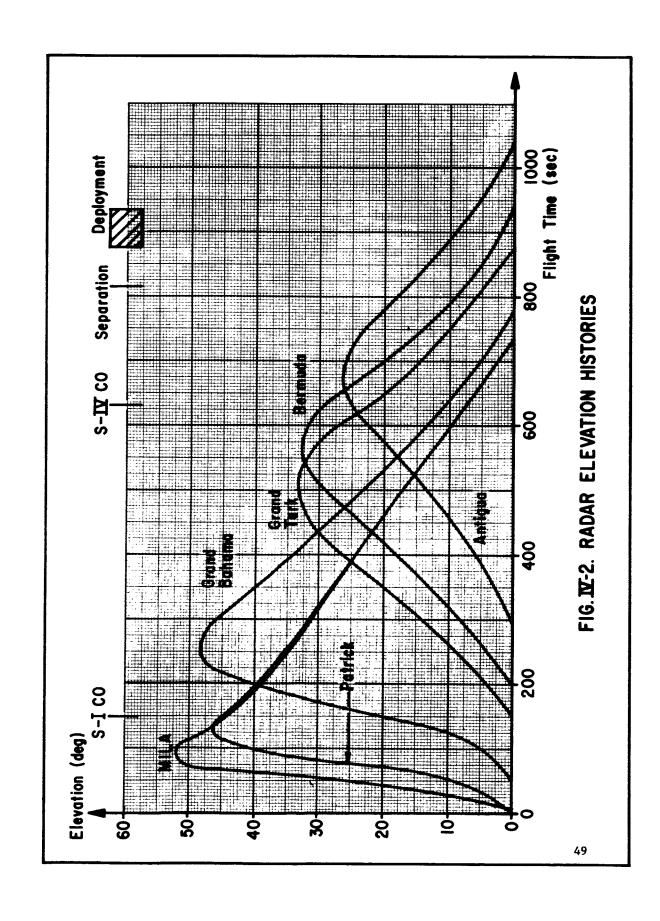
	Rev	7 1	Rev	2	Rev	7 3	Rev	4	Rev	5	
	€ *	R*	€	R	€	R	€	R	€	R	
RADAR	deg	km	deg	km	deg	km	deg	km	deg	km	
MILA	44	739	13	1574							
Patrick	45	725	14	1558							
Antigua	83	537	15	1457							
Bermuda	13	1607									
Ascension	19	1301	66	573	14	1532					
Carnarvon	68	561	18	1338							
Hawaii	75	550	39	803	31	950	53	654	42	761	
White Sands	50	685	27	1044							
Pretoria	33	887	81	533	54	635	84	528	31	923	
MINITRACK											
Ft. Myers	63	597	18	1343							
Quito			19	1310	66	574	11	1681			
Lima					24	1105	53	646			
Santiago							12	1638			
Johannesburg Woomera	32	904	82	5 32	54	639	81	531	33	895	
Goldstone	33	902	25	1103							

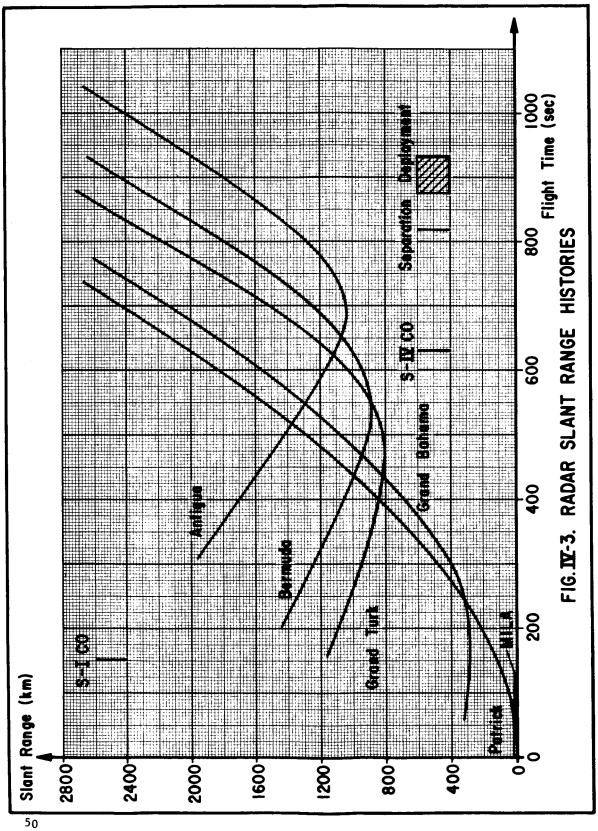
^{★ ∈} Maximum Elevation Angle

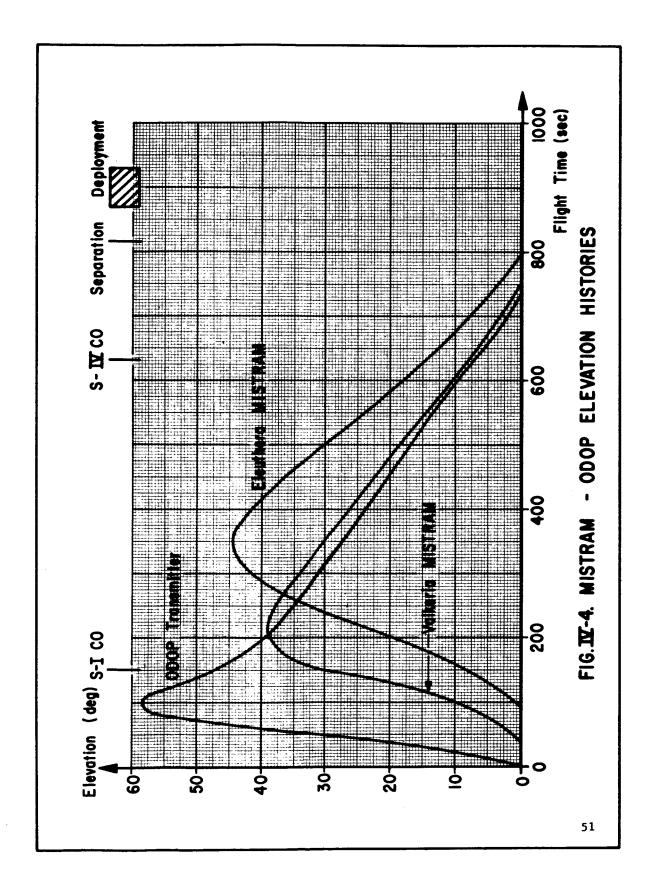
^{*} R Close Approach Range

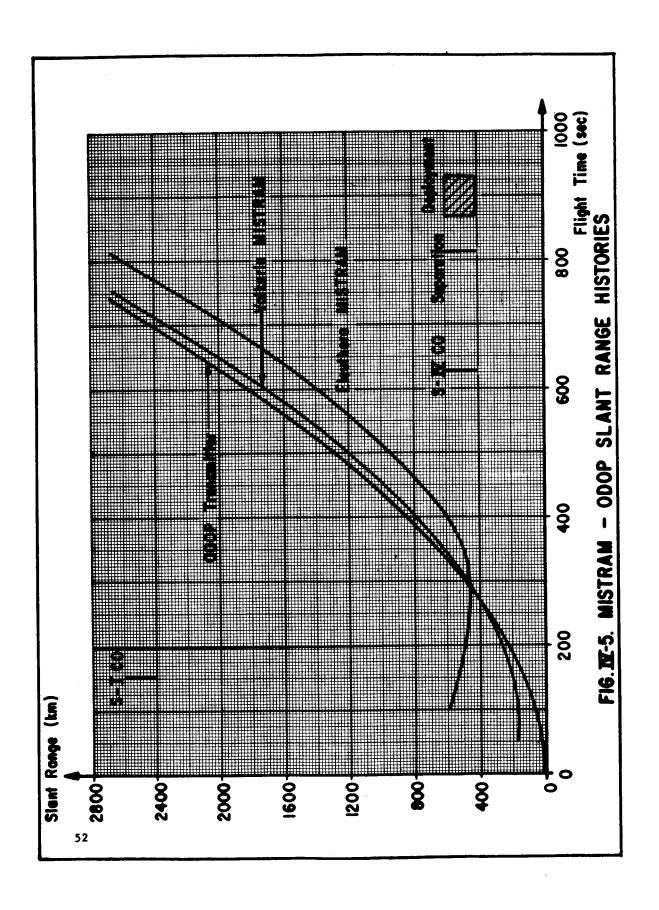
The Green Mountain station will view the first orbital pass 99 minutes after liftoff at zero deg elevation, an azimuth of 263 deg East-of-North and a slant range of 2671 km. Time above zero deg elevation will be 11 minutes. The close apprach range will be 1180 km at a maximum elevation of 22 deg.

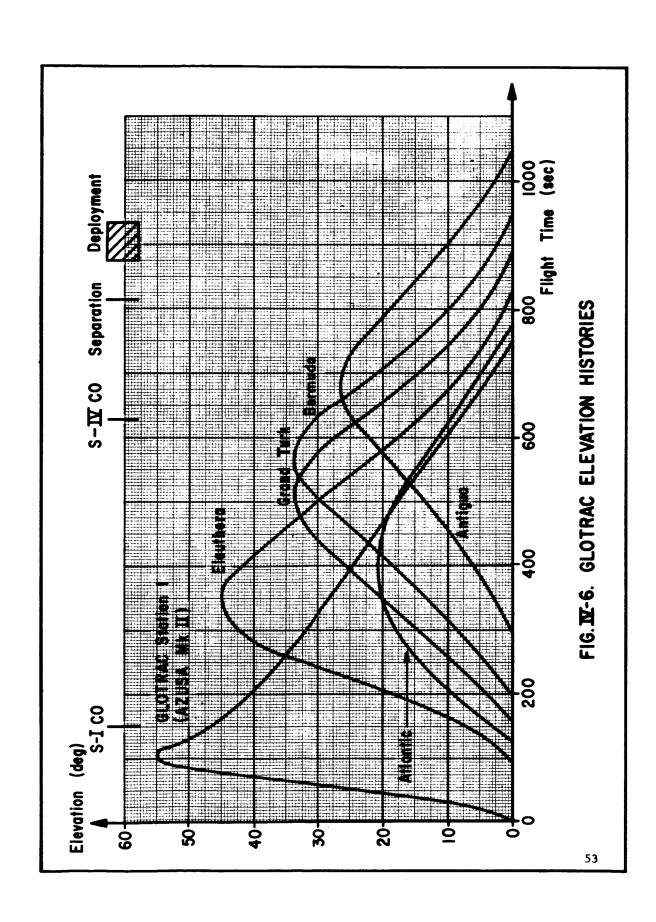


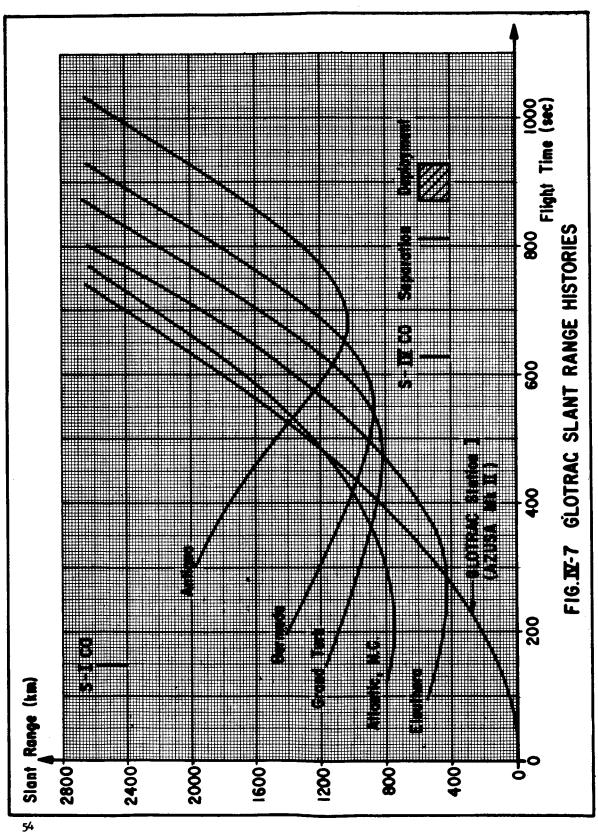


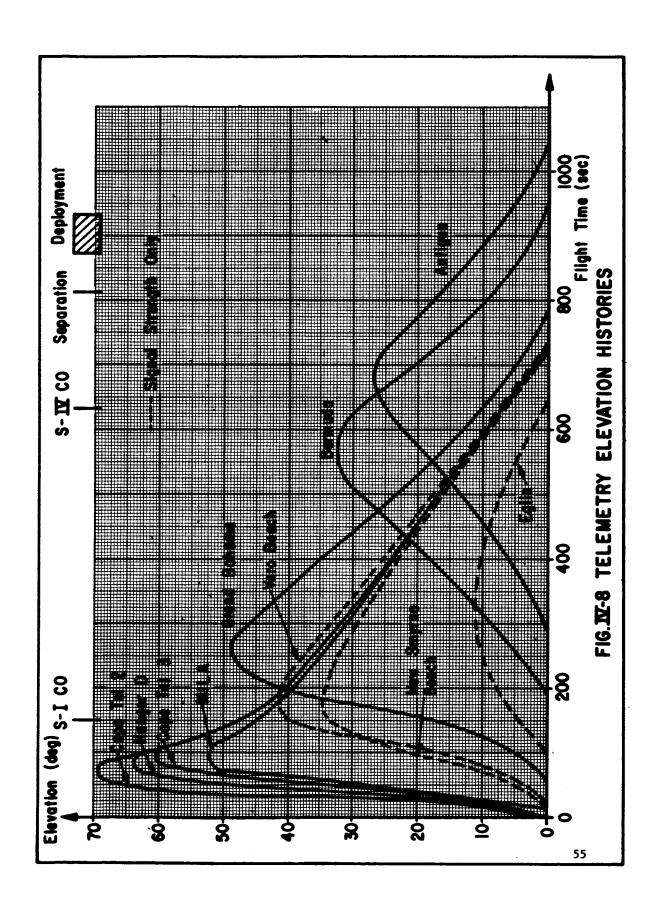


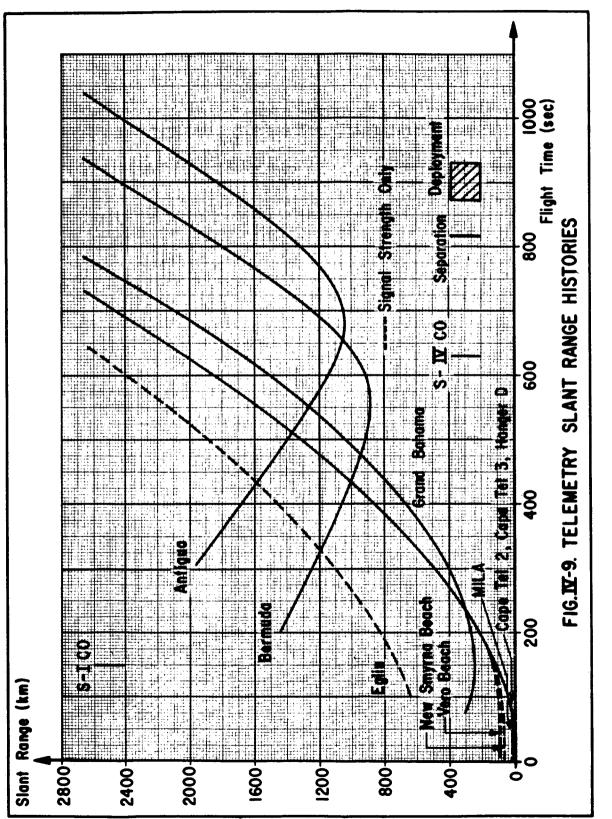


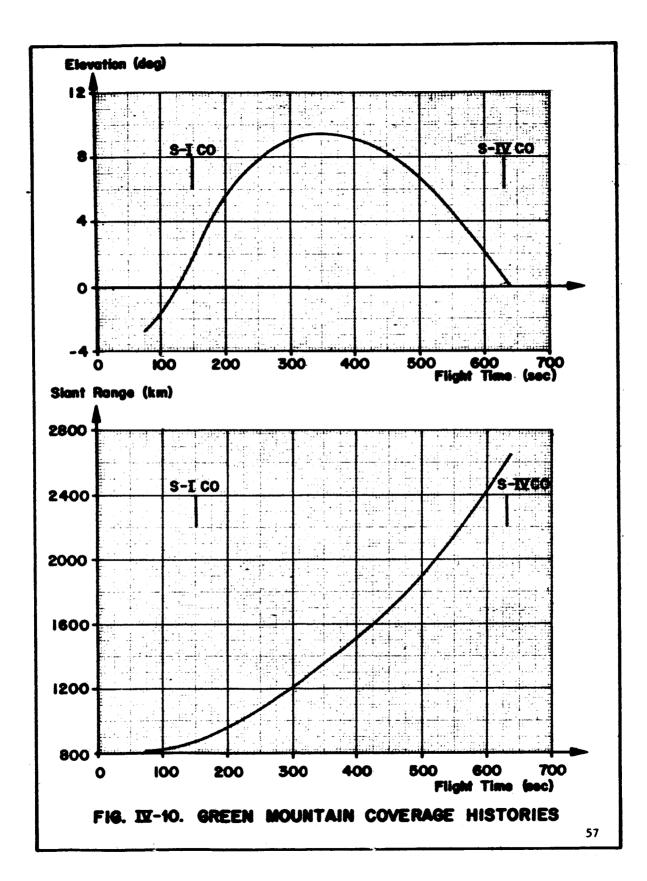


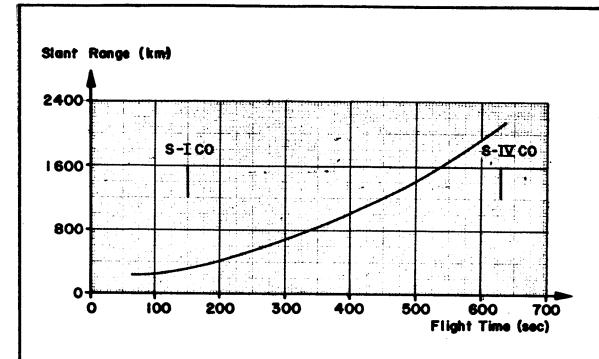












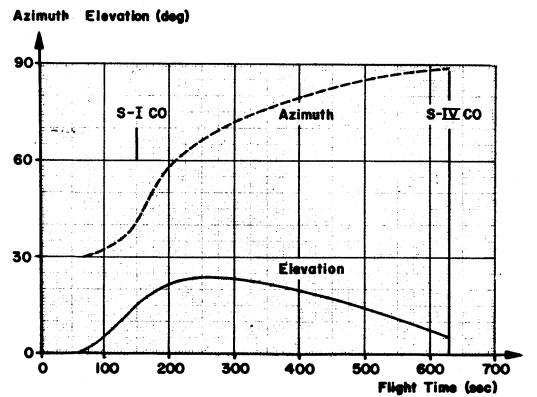
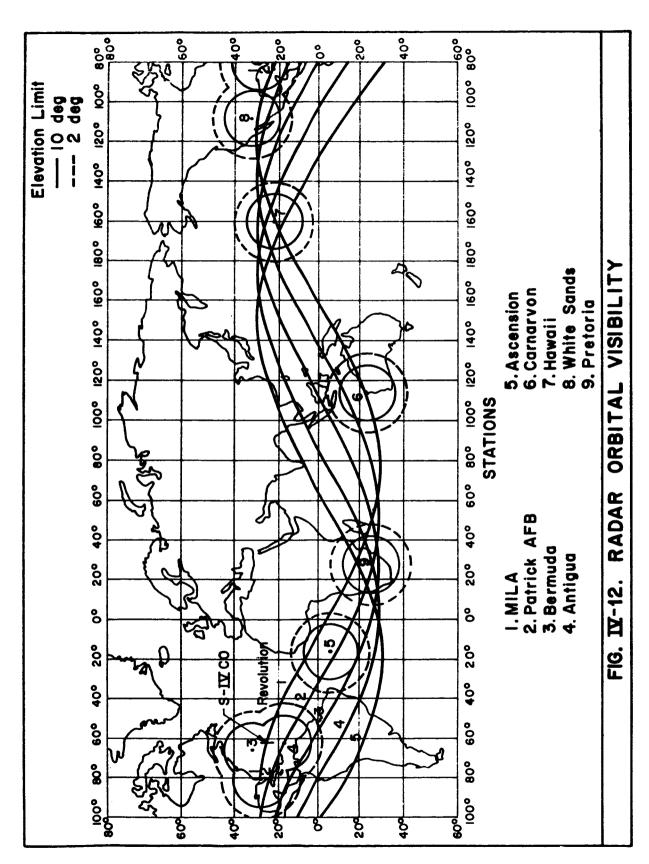
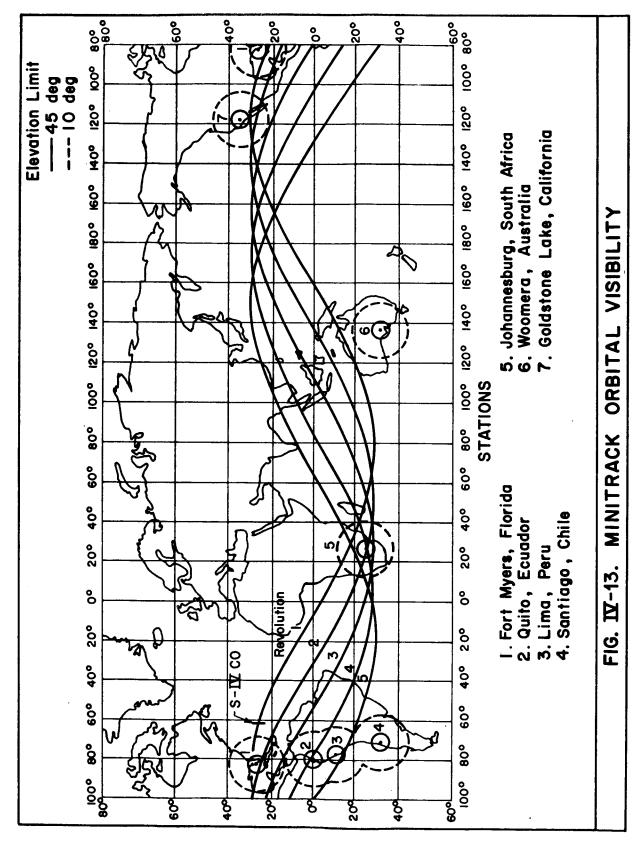


FIG. IX-11. FORT MYERS COVERAGE HISTORIES





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- 4. Saturn SA-10 Vehicle Data Book, June 11, 1965.
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- 7. Range Safety Report #4-65, June 17, 1965.

SA-10 FLIGHT MECHANICAL SUMMARY

The information in this report has been reviewed for security classification. Review of any information concerning Department of Defense or Atomic Energy Commission programs has been made by the MSFC Security Classification Officer. This report, in its entirety, has been determined to be unclassified.

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